

# Distinguished Lecturer 2024-25 Season



Recommended Practice for  
Safe Well Positioning,  
Separation, and Surveying



**Jonathan Lightfoot**  
Oxy

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# Recommended Practice for Safe Well Positioning, Separation, and Surveying

Jonathan Dale Lightfoot

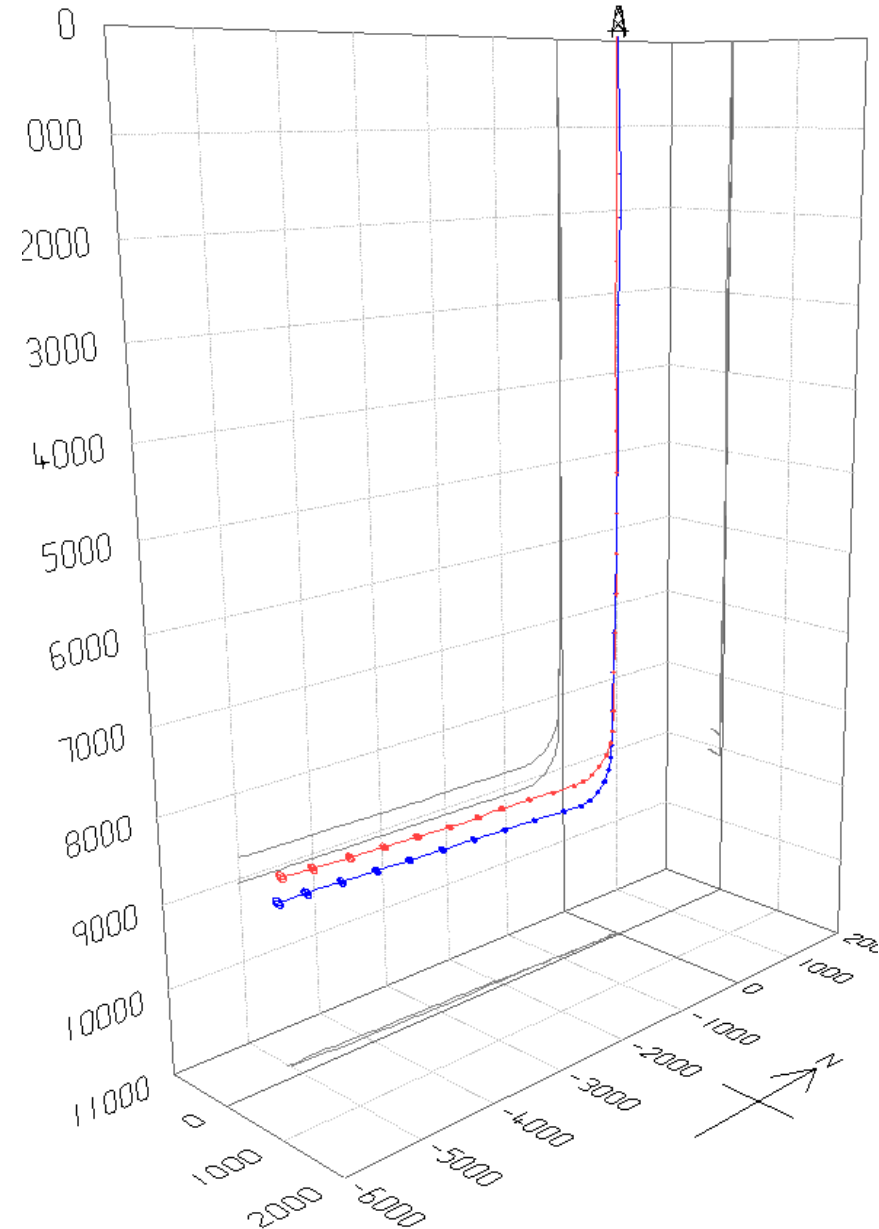


Society of Petroleum Engineers

Society of Petroleum Engineers  
Distinguished Lecturer Program  
[www.spe.org/dl](http://www.spe.org/dl)

# Presentation Outline

- **Safe Separation**
- **Applications**
- **Industry Collaboration**
- **Management Principles**
- **Position Uncertainty Models (PUMs)**
- **Offset Well Environment**
- **Case Studies**
  - **Offset Operator Close Approach**
  - **Lateral Undulations**
  - **Key Performance Indicators**
  - **Steerable Motor Curve**
  - **Lateral Tortuosity**
- **Key Takeaways**



# Safe Separation

## The Wellbore Positioning Technical Section (WPTS) Rule

Separation Factor = Ratio of Separation Distance and Uncertainty

Numerator  
Denominator

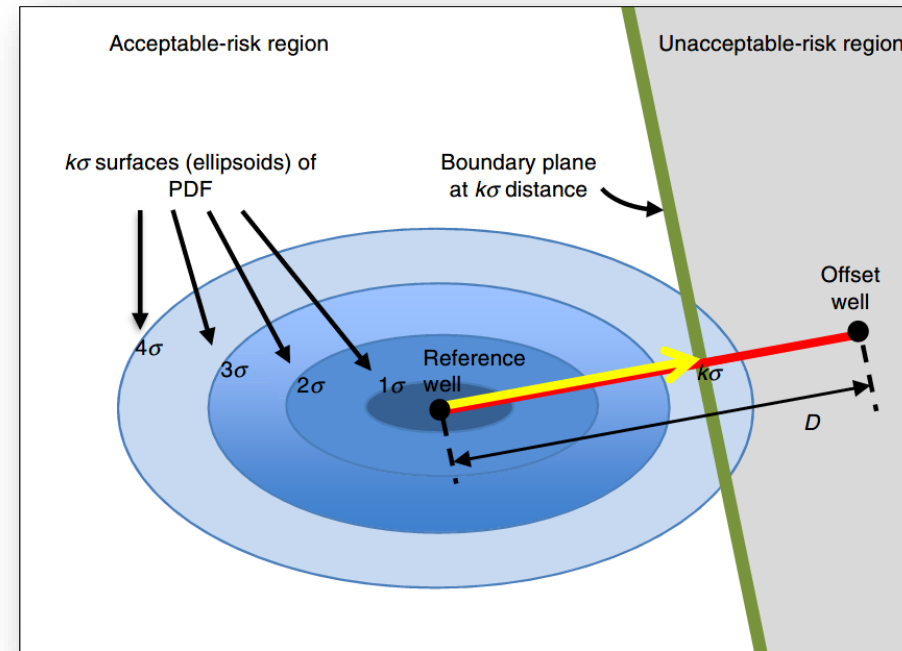


Distance  
Uncertainty

$$SF = \frac{D - R_r - R_o - S_m}{k \sqrt{\sigma_s^2 + \sigma_{pa}^2}}$$

$$\sqrt{\sigma_r^2 + \sigma_o^2}$$

$$k \sqrt{\sigma_s^2 + \sigma_{pa}^2}$$



# Applications

**Serves as the primary technical reference for proven engineering practice in the broad wellbore construction application of:**

- **Oil and Gas**
- **Geothermal**
- **Carbon Sequestration**
- **Coalbed Methane (CBM)**
- **Horizontal Directional Drilling (HDD), trenchless boring**
- **Mineral Ventilation and Extraction**
- **Scientific Coring**
- **All other subsurface borehole construction applications**

# Industry Collaboration

- **Industry Steering Committee on Wellbore Survey Accuracy**
  - Produces, maintains, and publishes standards for the industry
  - Promotes a collaborative understanding of issues associated with wellbore surveying
  - Formed in 1999, ISCWSA has been around for 29 Years [SPE 67616-PA]
  - 57 General Meetings
- **SPE Wellbore Positioning Technical Section (WPTS)**

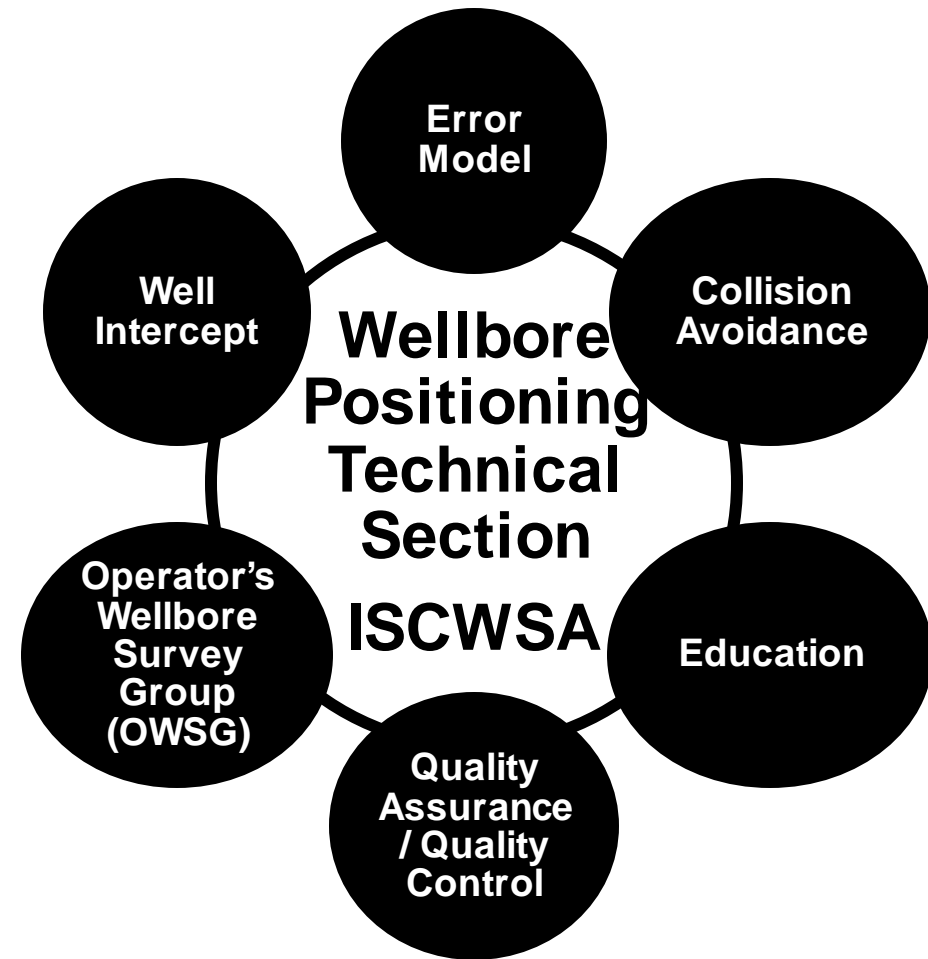


ISCWSA

# Industry Collaboration

WPTS has Six (6) Primary Sub-Committees

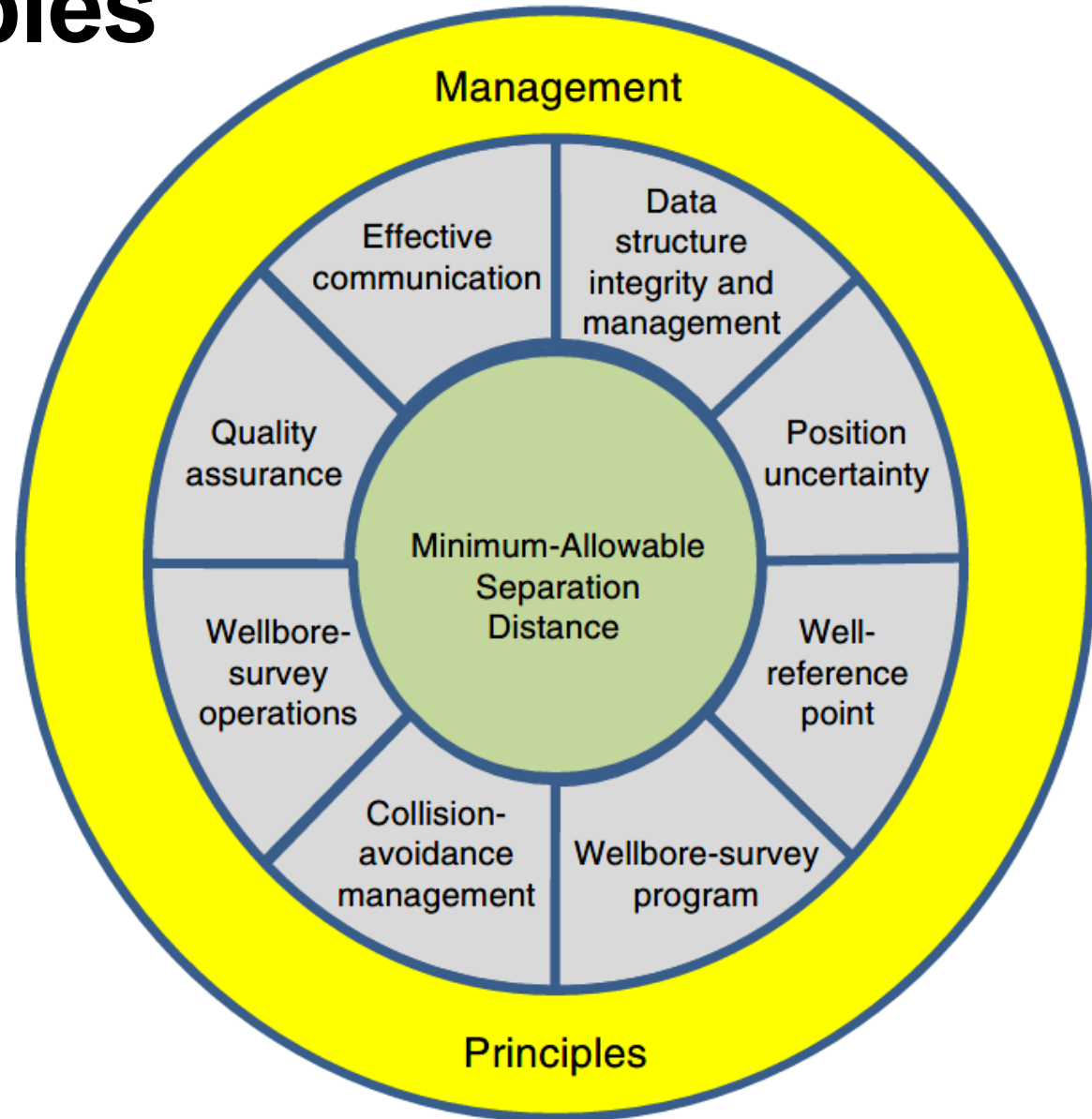
1. Collision Avoidance
2. Error Model Maintenance
3. Well Intercept
4. Operator's Wellbore Survey Group
5. Quality Assurance / Quality Control
6. Education





# Management Principles

- **Minimum Allowable Separation Distance (MASD)**
- **Maintain a Safe Separation Distance Between Wells Being Drilled and Subsurface Hazards**
- **8 Core MASD Elements**



The eight collision-avoidance elements supporting the MASD  
MASD Management Principles (SPE-187073-PA)

# Allowable Deviation from Plan for SF=1

Any given  $SF$  value represents a specific probability of the reference well crossing the offset well. The distance  $D$  at which a particular  $SF$  value occurs is situation specific. For any point on a reference well, the critical value  $SF = 1$  defines a minimum allowable separation distance (MASD) from the specified offset well along  $D$ :

$$SF = \frac{D - R_r - R_o - S_m}{k \sqrt{\sigma_s^2 + \sigma_{pa}^2}}$$

$$SF = \frac{D - R_r - R_o - 0.3}{3.5 \sqrt{\sigma_s^2 + 0.25}}$$

$$D_{MASD} = k \sqrt{\sigma_s^2 + \sigma_{pa}^2} + R_r + R_o + S_m$$

# Allowable Deviation from Plan for SF=1

$$D_{MASD} = k \sqrt{\sigma_s^2 + \sigma_{pa}^2} + R_r + R_o + S_m$$

If the distance  $D$  falls below  $D_{MASD}$ , then  $SF < 1$ . The difference between the planned distance  $D_{plan}$  and the  $D_{MASD}$  is the allowable deviation from the plan  $D_{ADP}$ :

$$D_{ADP} = D_{plan} - D_{MASD}$$

## SPE-187073-MS

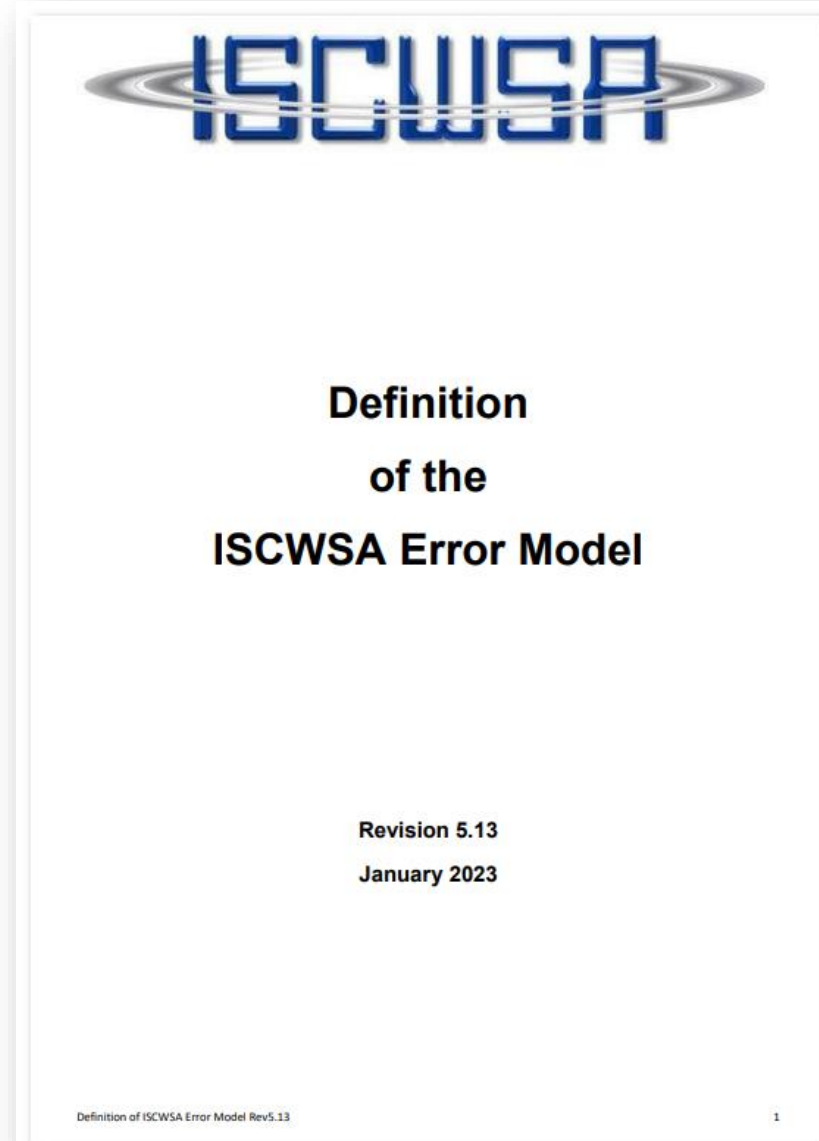
### Well Collision Avoidance - Separation Rule

S.J.Sawaryn, Consultant, H. Wilson, Baker Hughes a GE Company, J. Bang, Gyrodata Inc., E. Nymes, Statoil ASA, A. Sentance, Dynamic Graphics Inc., B. Poedjono and R. Lowdon, Schlumberger, I. Mitchell and J. Codling, Halliburton, P.J. Clark, Chevron Energy Technology, W.T. Allen, BP

## MASD Management Principles (SPE-187073-PA)

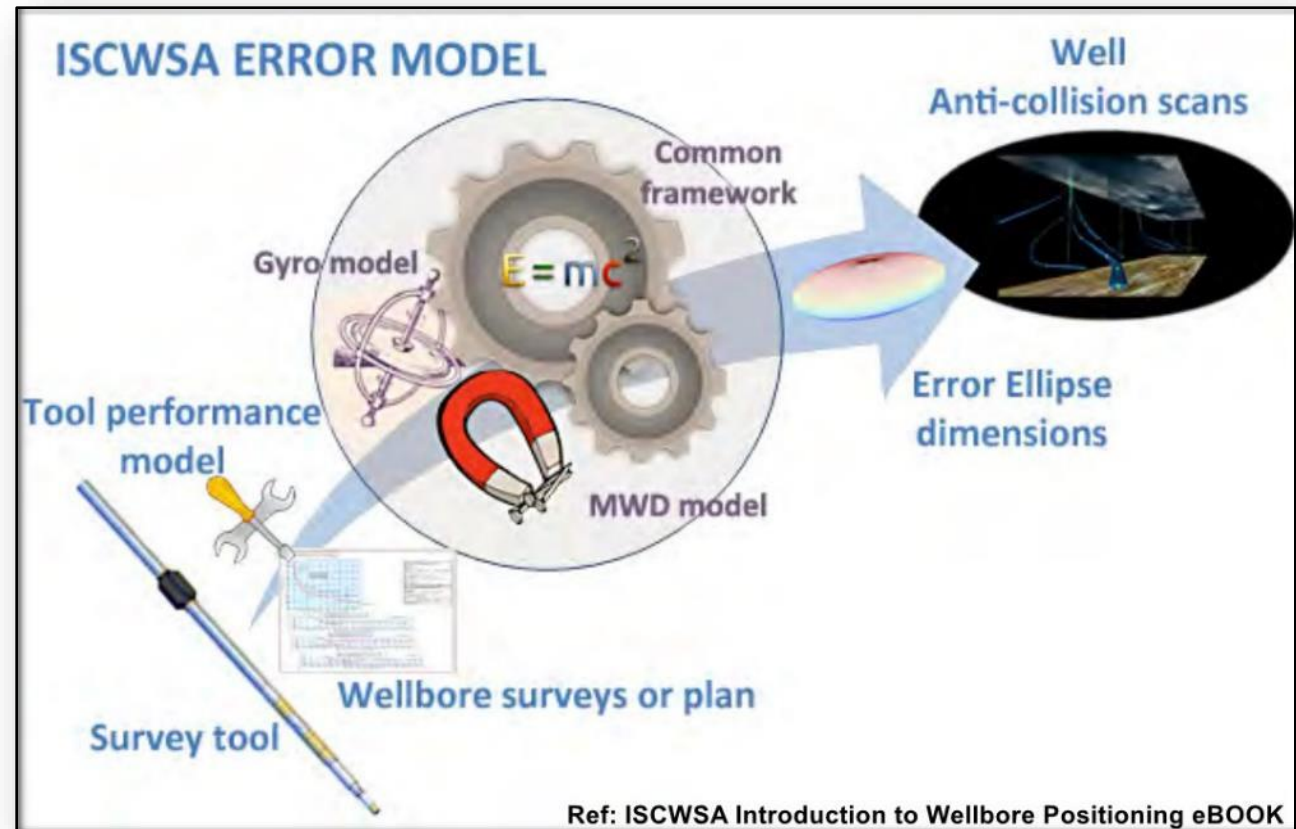
# Position Uncertainty Models (PUM)

**ISCWSA & OWSG Revisions**  
**PUM Categories**  
**Magnetic Reference**  
**Classification**  
**Generic Models (Set A & B)**  
**PUM Example – MWD + SRGM**  
**MWD Corrections**



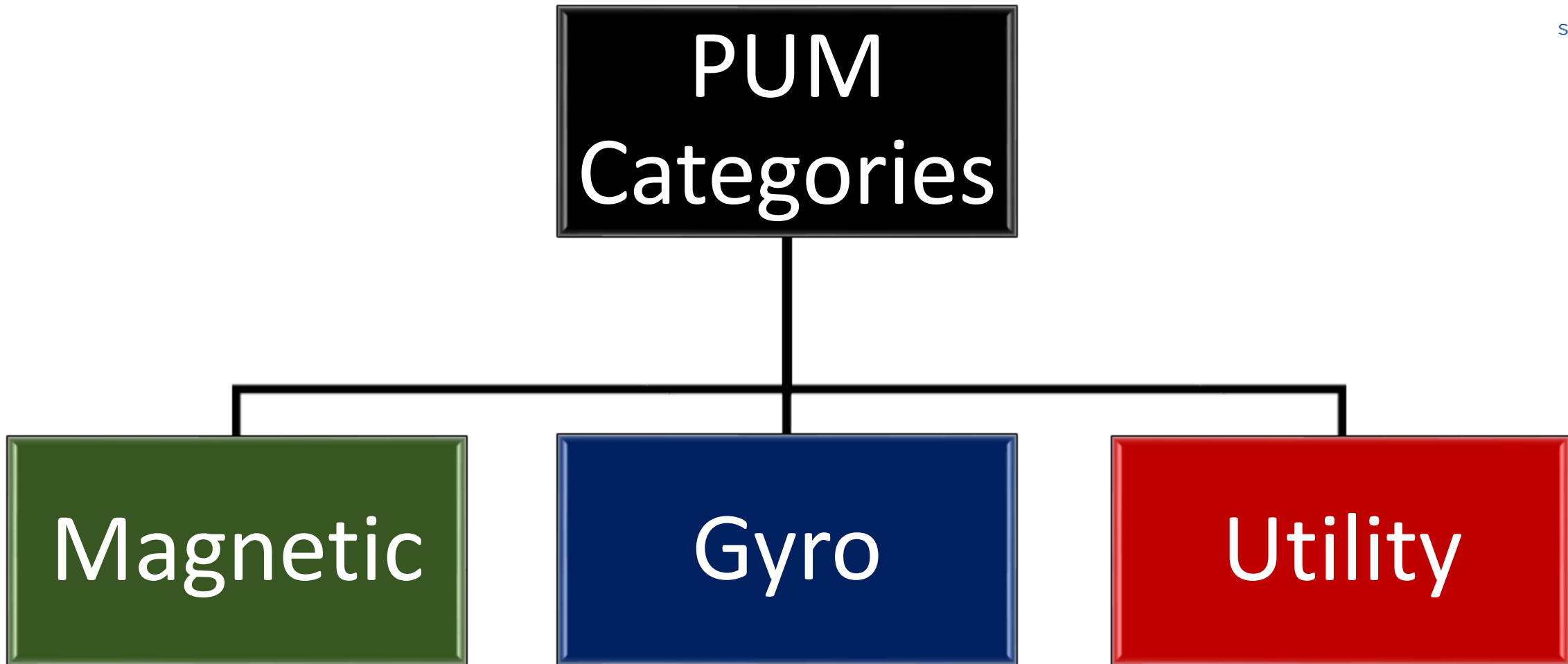
# PUM Sets – Established by OWSG

- PUM, often referred to as Error Models or Instrument Performance Models, Revision 5.13 (Current)
- Set A: Standard
- Set B: Extended
- Set C: Vendor-supplied
- Set D: Gyro software validation
- Set E: Prototypes in development

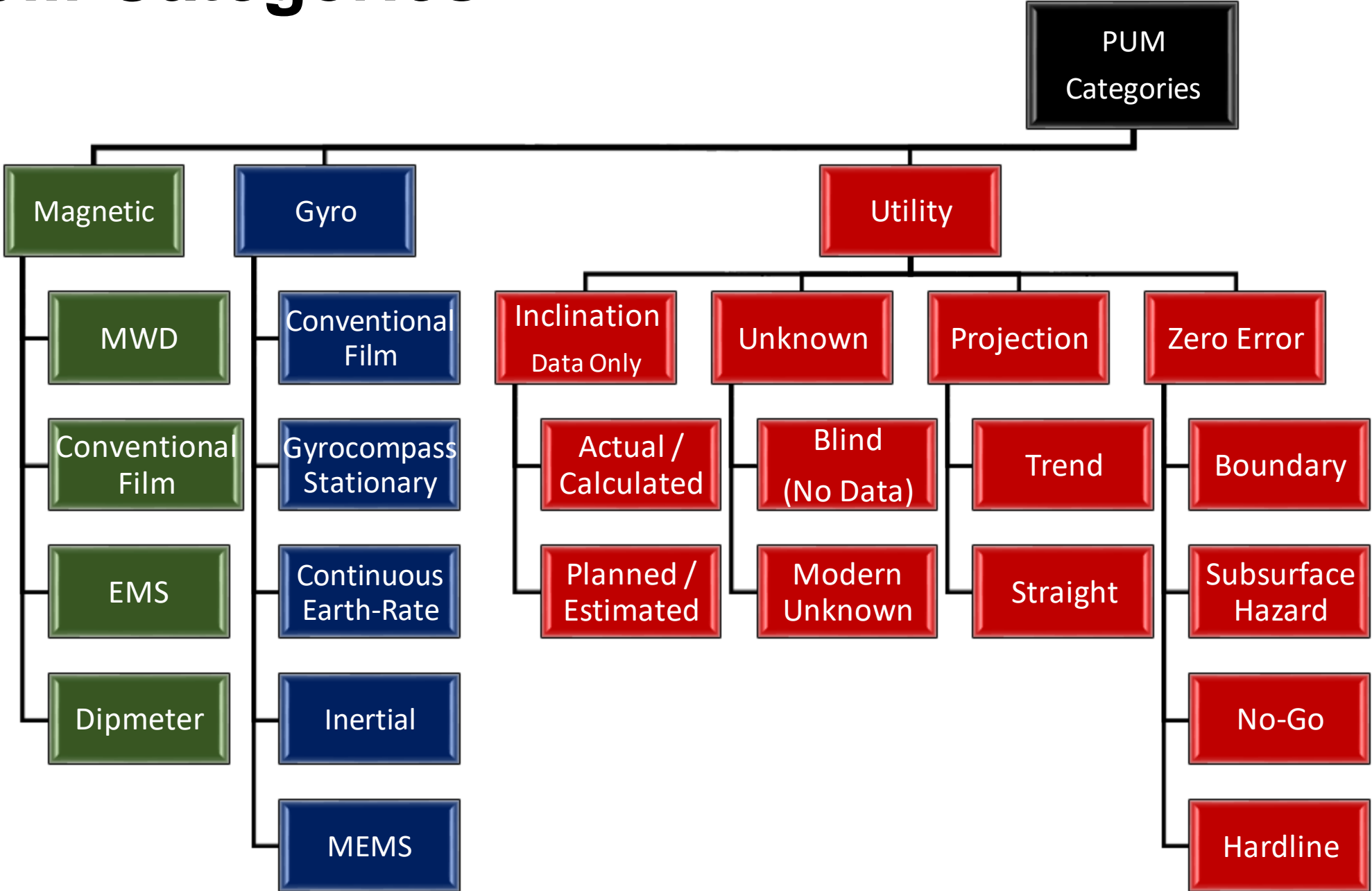


Grindrod, S. J., Clark, P. J., Lightfoot, J. D., Bergstrom, N., and L. S. Grant. "OWSG Standard Survey Tool Error Model Set for Improved Quality and Implementation in Directional Survey Management." Paper presented at the IADC/SPE Drilling Conference and Exhibition, Fort Worth, Texas, USA, March 2016. doi: <https://doi.org/10.2118/178843-MS>

# PUM Primary Categories

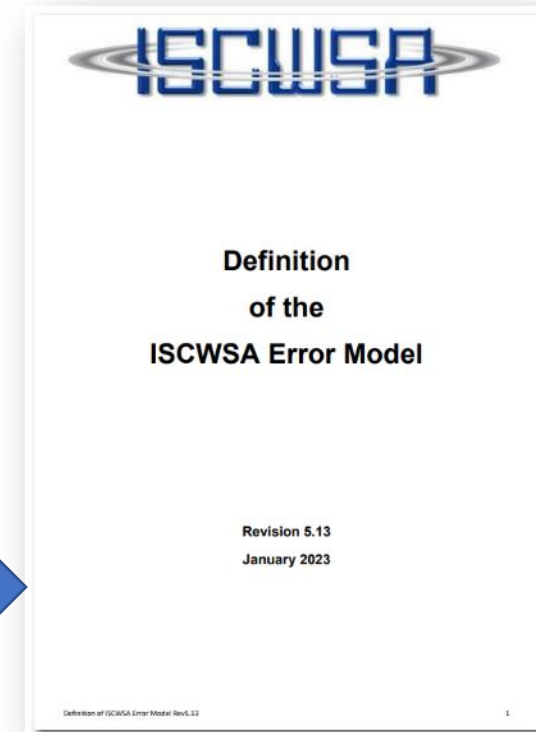


# PUM Categories



# Position Uncertainty Models (PUM)

Revision	Date	Description
Rev 0	Dec 2000	As per SPE 67616 together with various typographical corrections [1]
Rev 1	March 2005	Changed to the gyro style misalignment with 4 terms and calculation options [2]
Rev 2	Feb 2007	Changes to the parameter values for the depth scale and stretch terms [2]
Rev 3	Oct 2009	Replacement of all toolface dependent terms
Rev 4 & OWSG Rev 2	Mar 2019	Introduction of AMIL term and changes to misalignment magnitudes. Random magnetic reference values introduced to the main MWD model. OWSG includes Conventional, Gyro and Utility PUMs. Included Low Resolution and High Resolution Magnetic Reference Models for MWD and EMS. [3]
Rev 5	Oct 2020	Introduction of the XCL term, changes to misalignments and sag, breakout of magnetic reference terms and clarification of the surface tie-on. [4]
Rev 5.13	Jan 2023	Minor updates to Rev 5 [4] – Latest Revision



## Document Links

1. <https://doi.org/10.2118/67616-PA>
2. <https://doi.org/10.2118/105558-MS>
3. <https://doi.org/10.2118/178843-MS>
4. <https://www.iscwsa.net/media/files/files/64bd61c2/definition-of-iscwsa-error-model-v5-13.pdf>



# Magnetic Reference PUM Classification

Category	Abbreviation	Example Geomagnetic Models	Wavelength from 40,000 km Coverage	Update Frequency
Low Resolution	LRGM	GRF, WMM, CGRF	$\leq 4000$ km	Less than Annual
Standard Resolution	SRGM	MVSD, Pre-BGGM2019	$\leq 300$ km	Annual
High Resolution	HRGM	HDGM, MVHD, BGGM2019+, HDGM-RT	$\leq 55$ km	Annual
In-Field Referencing	IFR1	IFR, IFR1, Ground shot plus secular variation correction	$\leq 2$ km	Annual
In-Field Referencing with Realtime Disturbance Field Correction	IFR2	IFR2, IIFR	$\leq 2$ km plus local realtime ( $\leq 1$ min) sampling	Annual

Multiplier	Category
1.21	LRGM
1.00	SRGM
0.82	HRGM

# PUM Toolcodes Rev 5-1

A default set of conservative PUM tool-codes for use when tool specific models are not available.

- [ISCWSA Generic Toolcodes SetA Rev5-1](#)  
(updated Sept 23, 2022)
- [ISCWSA Generic Toolcodes SetB Rev5-1](#)  
(updated Sept 23, 2022)
- **Header / Reference Info**
- **Weighting Functions**
- **Technical Reference / Source**
- **Code & Term Description**
- **Type, Magnitude & Units**
- **Correlation Coefficients & Comments**
- **Formulas (Inclination & Azimuth)**

	OWSG Prefix	Short Name	Long Name
1	A001Mc	MWD+SRGM	OWSG MWD + SRGM
3	A002Mc	MWD+SRGM+SAG	OWSG MWD + SRGM + Sag Correction
5	A003Mc	MWD+SRGM+AX	OWSG MWD + SRGM + Axial Correction
7	A004Mc	MWD+SRGM+AX+SAG	OWSG MWD + SRGM + Axial Correction + Sag Correction
9	A005Mc	MWD+IFR1	OWSG MWD + IFR1
11	A006Mc	MWD+IFR1+AX	OWSG MWD + IFR1 + Axial Corr
13	A007Mc	MWD+IFR1+AX+SAG	OWSG MWD + IFR1 + Axial Corr + Sag Correction

	OWSG Prefix	Short Name	Long Name
1	B001Mc	MWD+HRGM	OWSG MWD + HRGM
3	B002Mc	MWD+HRGM+AX	OWSG MWD + HRGM + Axial Correction
5	B003Mc	MWD+HRGM+AX+SAG	OWSG MWD + HRGM + Axial Correction + Sag Correction
7	B004Mc	MWD+HRGM+SAG	OWSG MWD + HRGM + Sag Correction
9	B005Mc	MWD+HRGM+SAG+MS	OWSG MWD + HRGM + Sag + Multi-Station Correction
11	B006Mc	MWD+LRGM	OWSG MWD + LRGM
13	B007Mc	MWD+LRGM+AX	OWSG MWD + LRGM + Axial Correction
15	B008Mc	MWD+LRGM+AX+SAG	OWSG MWD + LRGM + Axial Correction + Sag Correction
17	B009Mc	MWD+LRGM+SAG	OWSG MWD + LRGM + Sag Correction
19	B010Mc	EMS+IFR1+AX+SAG	OWSG EMS + IFR1 + Axial Corr + Sag Correction
21	B011Mc	EMS+IFR1+SAG	OWSG EMS + IFR1 + Sag Correction
23	B012Mc	EMS+IFR1+SAG+MS	OWSG EMS + IFR1 + Sag + Multi-Station Correction
25	B013Mc	EMS+HRGM	OWSG EMS + HRGM
27	B014Mc	EMS+HRGM+AX	OWSG EMS + HRGM + Axial Correction
29	B015Mc	EMS+HRGM+AX+SAG	OWSG EMS + HRGM + Axial Correction + Sag Correction
31	B016Mc	EMS+HRGM+SAG	OWSG EMS + HRGM + Sag Correction
33	B017Mc	EMS+LRGM	OWSG EMS + LRGM
35	B018Md	EMS+LRGM+AX	OWSG EMS + LRGM + Axial Correction
37	B019Md	EMS+LRGM+AX+SAG	OWSG EMS + LRGM + Axial Correction + Sag Correction
39	B020Mc	EMS+LRGM+SAG	OWSG EMS + LRGM + Sag Correction
41	B021Ga	FINDS	OWSG BHI Ferranti FINDS
42	B022Ua	BLIND+TREND	OWSG BLIND+TREND

Set B  
Extended

# Example: A001Mc MWD+SRGM



<https://www.iscwsa.net/error-model-documentation/>  
[ISCWSA Generic Toolcodes SetA Rev5-1](#) (updated 23/9/22)

Excel Workbook Tab: MWD+SRGM

A001Mc MWD-SRGM		No Code	Term Description	Vt.Fn.	Vt.Fn. Source	Type	Magnitude	Units	Prop.	P1	P2	P3	Vt.Fn. Comment	Depth	Form	Inclination	Formula	Azimuth	Formula
01	DFFF	Depth: Depth Reference - Random	DREF	SPE 67616	Depth	0.35	m	R	0	0	0	0		1	0	0		0	
02	DSFS	Depth: Depth Scale Factor - Systematic	DSF	SPE 67616	Depth	0.00056	-	S	1	0	0	0		MD	0	0		0	
03	DSTG	Depth: Depth Stretch - Global	DST	SPE 67616	Depth	0.00000025	1/m	G	1	1	1	1		MD * TVD	0	0		0	
04	ABXY-T16	MWD TF Ind: X and Y Accelerometer Bias	ABXY-T16	SPE 63275 - Andy Broo	Sensor	0.004	m/s2	S	1	0	0	0		0	0	-Cos(Inc) / Gfield		(Tan(Dip) * Cos(Inc) * Sin(AzM)) / Gfield	
05	ABXY-T12	MWD TF Ind: X and Y Accelerometer Bias	ABXY-T12	SPE 63275 - Andy Broo	Sensor	0.004	m/s2	S	1	0	0	0	Singularity when vertical	0	0			((Tan((pi / 2) - Inc)) - Tan(Dip) * Cos(AzM)) / Gfield	
06	ABZ	MWD: Z-Accelerometer Bias	ABZ	SPE 67616 Table 1	Sensor	0.004	m/s2	S	1	0	0	0		0	0	-Sin(Inc) / Gfield		Tan(Dip) * Sin(Inc) * Sin(AzM) / Gfield	
07	ASXY-T16	MWD TF Ind: X and Y Accelerometer Scale Factor	ASXY-T16	SPE 63275 - Andy Broo	Sensor	0.0005	-	S	1	0	0	0		0	0	Sin(Inc) * Cos(Inc) / Sqr(2)		(-Tan(Dip) * Sin(Inc) * Cos(Inc) * Sin(AzM)) / Sqr(2)	
08	ASXY-T12	MWD TF Ind: X and Y Accelerometer Scale Factor	ASXY-T12	SPE 63275 - Andy Broo	Sensor	0.0005	-	S	1	0	0	0		0	0	(Tan(Dip) * Sin(Inc) * Cos(Inc) * Sin(AzM)) / 2		(Tan(Dip) * Sin(Inc) * Cos(Inc) * Sin(AzM)) / 2	
09	ASXY-T13	MWD TF Ind: X and Y Accelerometer Scale Factor	ASXY-T13	SPE 63275 - Andy Broo	Sensor	0.0005	-	S	1	0	0	0		0	0	(Tan(Dip) * Sin(Inc) * Cos(Inc) * Sin(AzM)) / 2		(Tan(Dip) * Sin(Inc) * Cos(Inc) * Sin(AzM)) / 2	
10	ASZ	MWD: Z-Accelerometer Scale Factor	ASZ	SPE 67616 Table 1	Sensor	0.0005	-	S	1	0	0	0		0	0			(Tan(Dip) * Sin(Inc) * Cos(Inc) * Sin(AzM))	
11	MBXY-T11	MWD TF Ind: X and Y Magnetometer Bias	MBXY-T11	SPE 63275 - Andy Broo	Sensor	70	nT	S	1	0	0	0		0	0			(Cos(Inc) * Sin(AzM)) / (BField * Cos(Dip))	
12	MBXY-T12	MWD TF Ind: X and Y Magnetometer Bias	MBXY-T12	SPE 63275 - Andy Broo	Sensor	70	nT	S	1	0	0	0		0	0			Cos(AzM) / (BField * Cos(Dip))	
13	MBZ	MWD: Z-Magnetometer Bias	MBZ	SPE 67616 Table 1	Sensor	70	nT	S	1	0	0	0		0	0			-Sin(Inc) * Sin(AzM) / (BField * Cos(Dip))	
14	MSXY-T11	MWD TF Ind: X and Y Magnetometer Scale Factor	MSXY-T11	SPE 63275 - Andy Broo	Sensor	0.0016	-	S	1	0	0	0		0	0			Sin(Inc) * Sin(AzM) * (Tan(Dip) * Cos(Inc) * Sin(AzM) + Cos(AzM))	
15	MSXY-T12	MWD TF Ind: X and Y Magnetometer Scale Factor	MSXY-T12	SPE 63275 - Andy Broo	Sensor	0.0016	-	S	1	0	0	0		0	0			Sin(Inc) * Sin(AzM) * (Tan(Dip) * Sin(Inc) * Cos(Inc) * Sin(AzM) + Cos(AzM))	
16	MSXY-T13	MWD TF Ind: X and Y Magnetometer Scale Factor	MSXY-T13	SPE 63275 - Andy Broo	Sensor	0.0016	-	S	1	0	0	0		0	0			Sin(Inc) * Sin(AzM) * (Tan(Dip) * Sin(Inc) * Cos(Inc) * Sin(AzM) + Cos(AzM))	
17	MSZ	MWD: Z-Magnetometer Scale Factor	MSZ	SPE 67616 Table 1	Sensor	0.0016	-	S	1	0	0	0		0	0			(Tan(Dip) * Sin(Inc) * Cos(Inc) * Sin(AzM) + Cos(AzM)) * Sin(AzM)	
18	DEC-O	MWD: Declination Crustal Omission Error Models	AZ	SPE 67616	AziRef	0.05	deg	G	1	1	1	1		0	0	0	0	1	Sin(Inc) * Cos(AzM) / (BField * Cos(Dip))
19	DEC-OS	MWD: Declination Crustal Omission Error Models	AZ	SPE 67616	AziRef	0.05	deg	G	1	1	1	1		0	0	0	0	1	Sin(Inc) * Cos(AzM) / (BField * Cos(Dip))
20	DEC-OH	MWD: Declination Crustal Omission HD Models	AZ	SPE 67616	AziRef	0.21	deg	G	1	1	1	1		0	0	0	0	1	Sin(Inc) * Cos(AzM) / (BField * Cos(Dip))
21	DEC-OI	MWD: Declination Crustal Omission IFR Models	AZ	SPE 67616	AziRef	0.05	deg	G	1	1	1	1		0	0	0	0	1	Sin(Inc) * Cos(AzM) / (BField * Cos(Dip))
22	DECR	MWD: Declination - Random	DECR	SPE 67616	AziRef	0.1	deg	R	0	0	0	0		0	0	0	0	1	Sin(Inc) * Cos(AzM) / (BField * Cos(Dip))
23	DBH-U	MWD: BH Dependent Declination Uncorrelated Errors	DBH	SPE 67616	AziRef	356	deg.nT	G	1	1	1	1		0	0	0	0	1	1 / (BField * Cos(Dip))
24	DBH-OS	MWD: BH Dependent Declination Crustal Omission Standard	DBH	SPE 67616	AziRef	356	deg.nT	G	1	1	1	1		0	0	0	0	1	1 / (BField * Cos(Dip))
25	DBH-OH	MWD: BH Dependent Declination Crustal Omission HD Models	DBH	SPE 67616	AziRef	356	deg.nT	G	1	1	1	1		0	0	0	0	1	1 / (BField * Cos(Dip))
26	DBH-OI	MWD: BH Dependent Declination Crustal Omission IFR Models	DBH	SPE 67616	AziRef	356	deg.nT	G	1	1	1	1		0	0	0	0	1	1 / (BField * Cos(Dip))
27	DBHR	MWD: BH-Dependent Declination - Random	DBH	SPE 67616	AziRef	3000	deg.nT	R	0	0	0	0		0	0	0	0	1	1 / (BField * Cos(Dip))
28	AMIL	MWD: Axial Interference - Sin(Az)Sin(Az)	AMIL	Halliburton	Mgmt	220	nT	S	1	0	0	0		0	0	0	0	0	Sin(Inc) * Sin(AzM) / (BField * Cos(Dip))
29	SAGE	MWD: Sag	SAGE	ISCWSA	Align	0.2	deg	S	1	0	0	0		0	0	0	0	0	(Sin(Inc))^0.25
30	XYM1	Misalignment: XY Misalignment 1	XYM1	SPE 90408 Table 9 - Alt.	Align	0.1	deg	S	1	0	0	0		0	0	0	0	0	Abs(Sin(Inc))
31	XYM2	Misalignment: XY Misalignment 2	XYM2	SPE 90408 Table 9 - Alt.	Align	0.1	deg	S	1	0	0	0		0	0	0	0	0	0
32	XYM3E	Misalignment: XY Misalignment 3	XYM3E	ISCWSA	Align	0.3	deg	R	0	0	0	0	Singularity when vertical	0	0	0	0	0	Cos(Inc) * Cos(AzT) * Max(1, sqrt(10) / (MD-MDPrev) * (Cos(Inc) * Sin(AzT) / Sin(Inc)) * Max(1, sqrt(10) / (MD-MDPrev)))
33	XYM4E	Misalignment: XY Misalignment 4	XYM4E	ISCWSA	Align	0.3	deg	R	0	0	0	0	Singularity when vertical	0	0	0	0	0	Cos(Inc) * Sin(AzT) * Max(1, sqrt(10) / (MD-MDPrev) * (Cos(Inc) * Cos(AzT) / Sin(Inc)) * Max(1, sqrt(10) / (MD-MDPrev)))
34	XCLA	Depth: Long Course Length XCL - Azimuth	XCLA	SPE 187249 Jerry Codlin	Depth	0.167	-	R	0	0	0	0	Tangential Calculation, Singularity when vertical	0	0	0	0	0	Max(Sin(Abs(AzT-AzPrev)), XCLTortuosity * (MD-MDPrev) / Sin(Inc))
35	XCLH	Depth: Long Course Length XCL - Inclination	XCLH	SPE 187249 Jerry Codlin	Depth	0.167	-	R	0	0	0	0	Tangential Calculation, Form	0	0	0	0	0	Max(Abs(Inc-IncPrev), XCLTortuosity * (MD-MDPrev) / Cos(Inc))

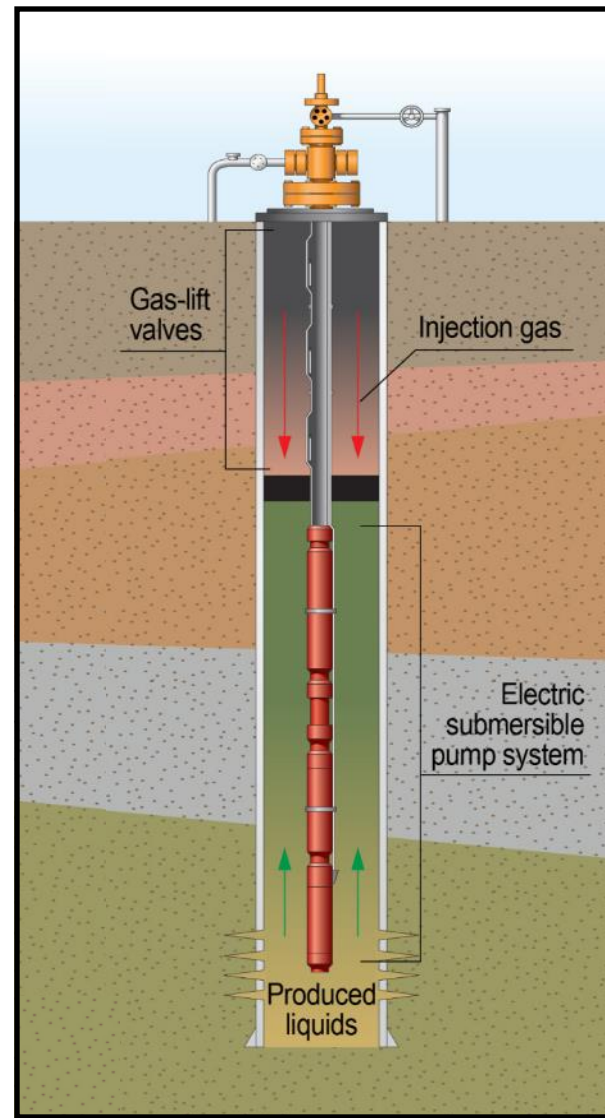
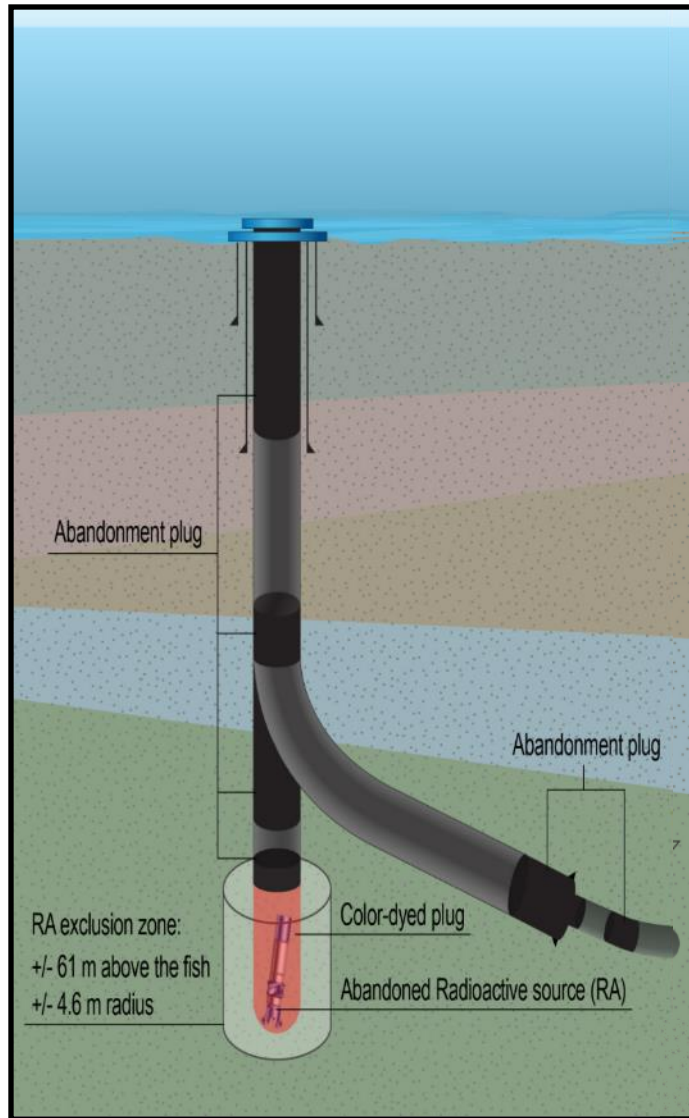
# Header Reference Information

# PUM Specification, Weighting Functions, & Calculations

# MWD PUM Survey Corrections

- **Axial (AX)**
- **Sag**
- **Multi-Station Analysis (MSA or MS)**
- **Axial + Sag**
- **Multi-Station + Sag**
- **Depth Corrections**
- **Advanced MWD Corrections**
  - **Ground Shot (GS) IFR**
  - **Advanced Multi-Station (AMSA)**
    - **All BHA's for a Wellbore**
    - **All BHA's for all wellbores on a well (Includes Sidetracks / By-Pass Wellbores)**
    - **All BHA's for all wellbores on a Site/Location/Pad**

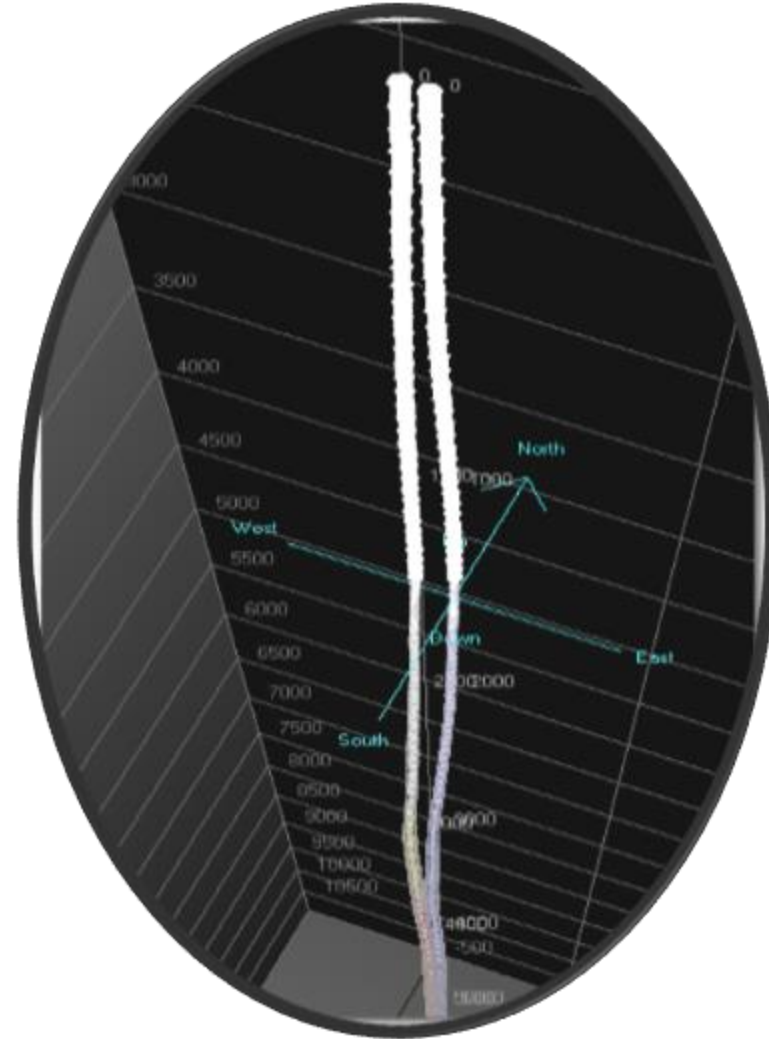
# Offset Well Environment



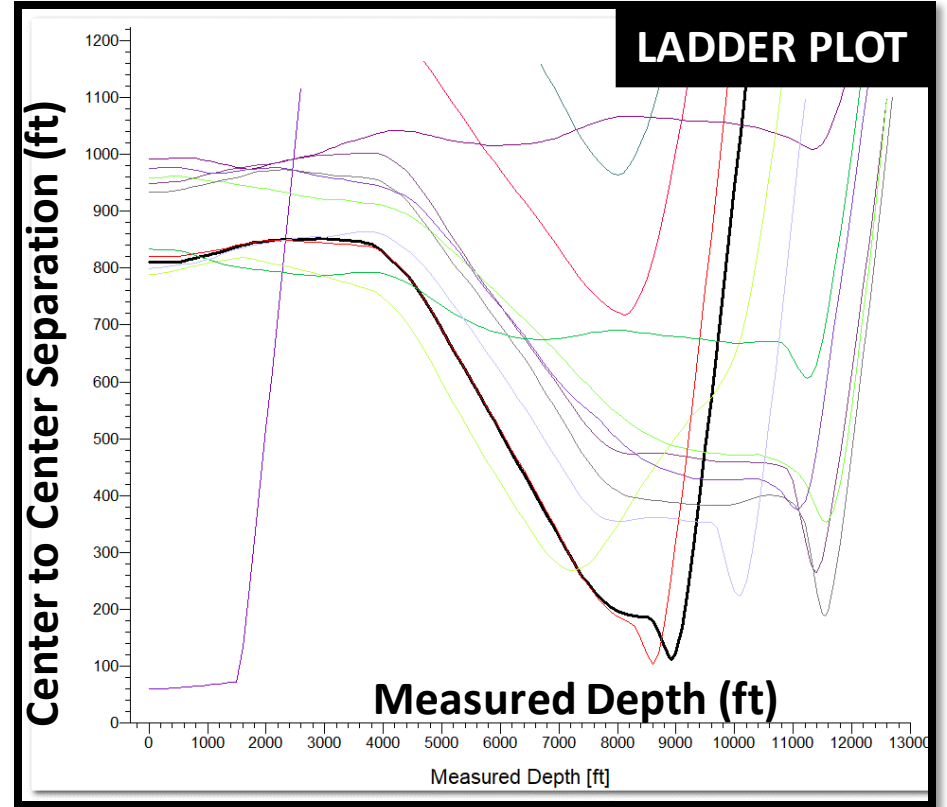
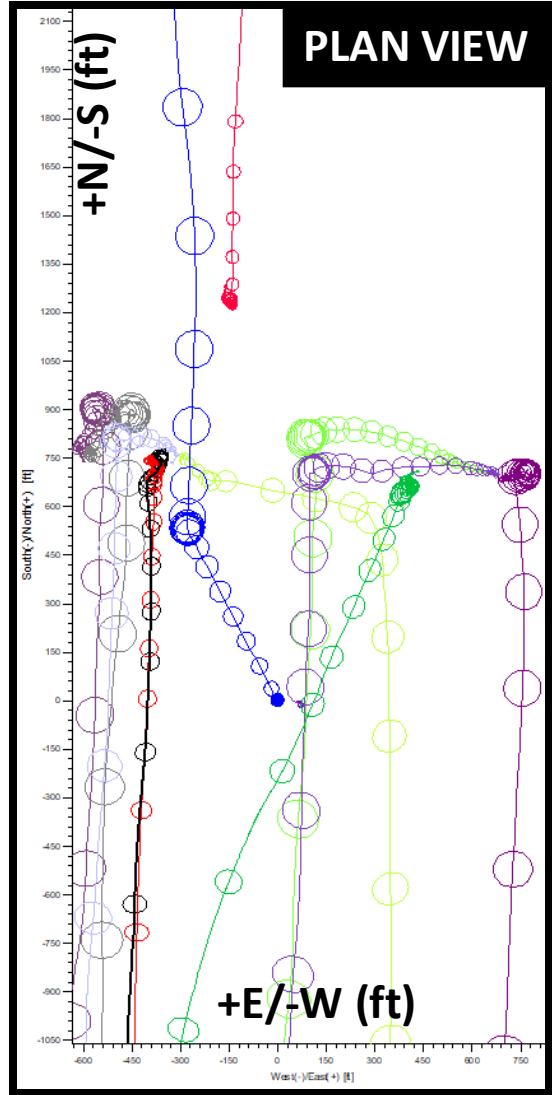
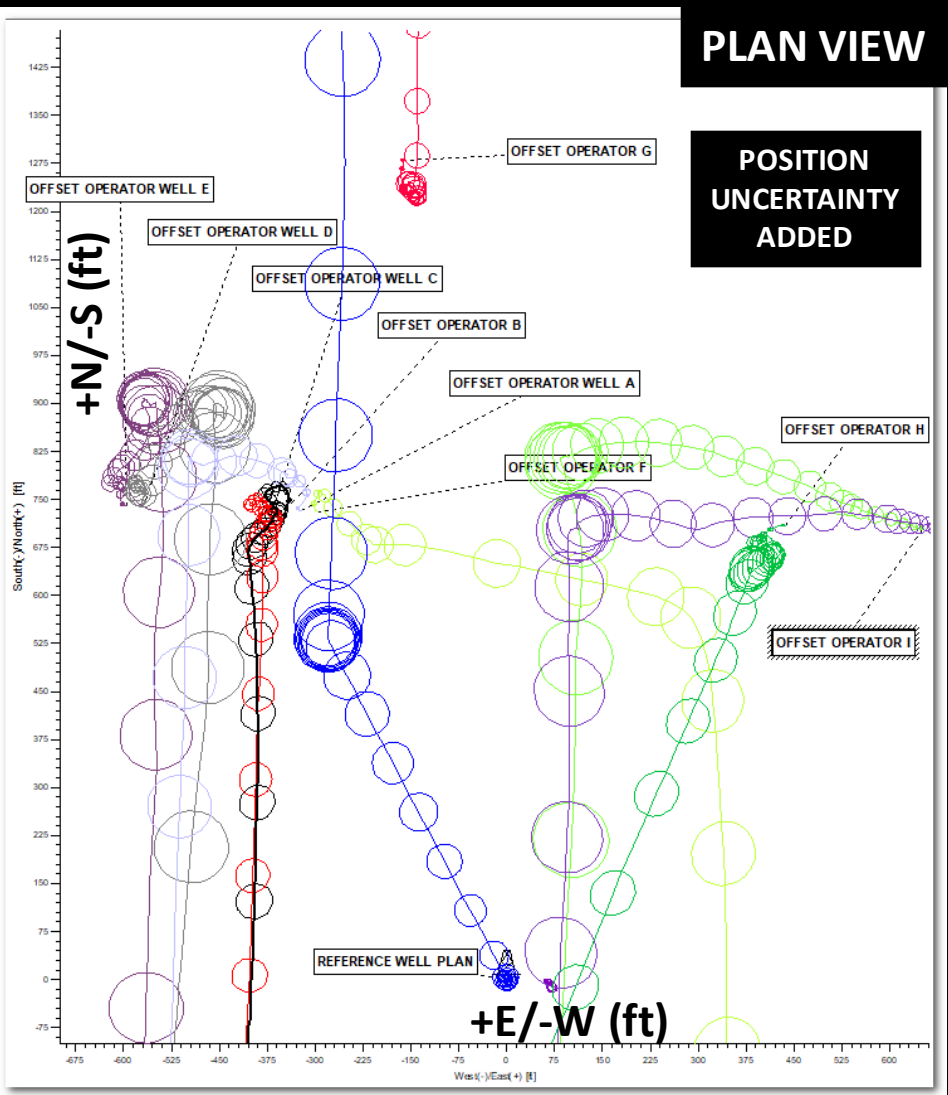
- **Offset Well Environment**
  - Status
  - Completion Type
  - Wellbore Fluids
  - Lifting Mechanism
- **Artificial Lift**
  - Rod Pump
  - Progressive Cavity
  - Hydraulic Pump
  - Gas Lift (GL)
  - Electric Submersible Pump (ESP)
  - Hybrid Lift System
    - GL & ESP
    - ESP & Natural Flow

# Case Study

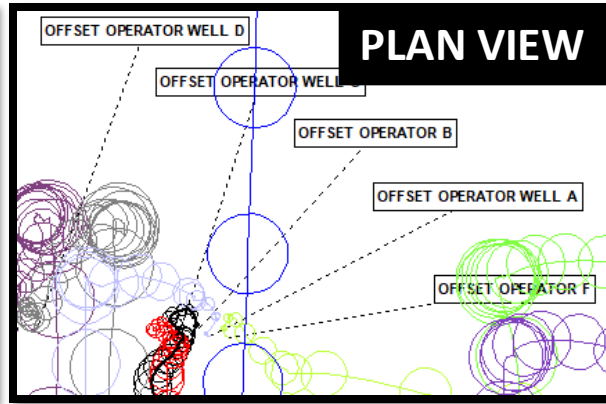
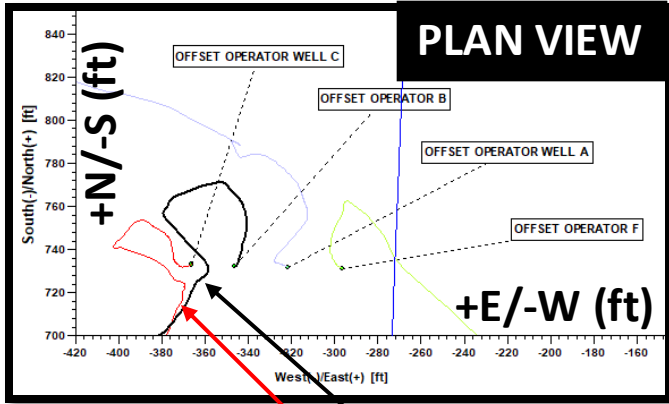
## Offset Operator Close Approach



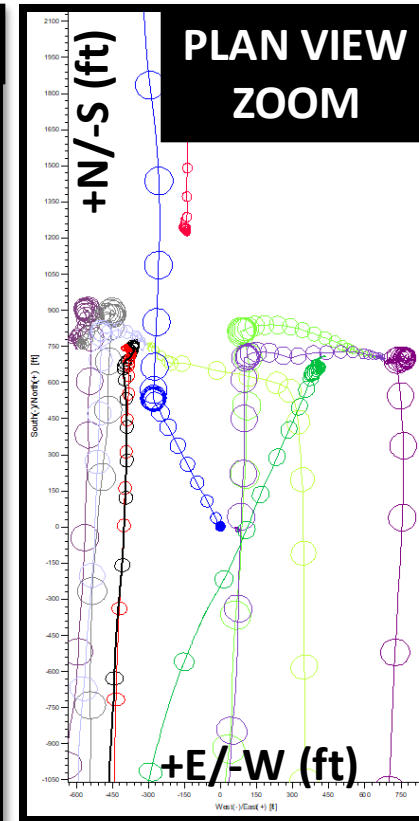
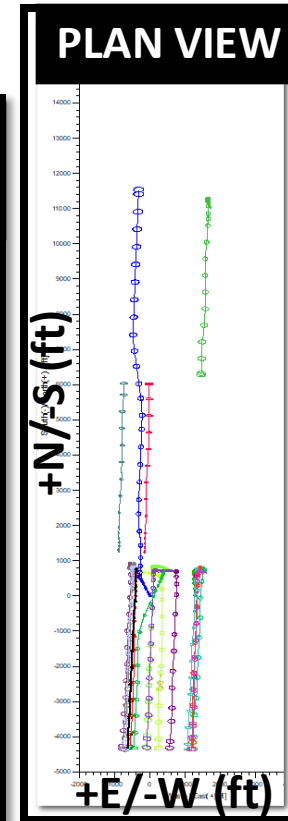
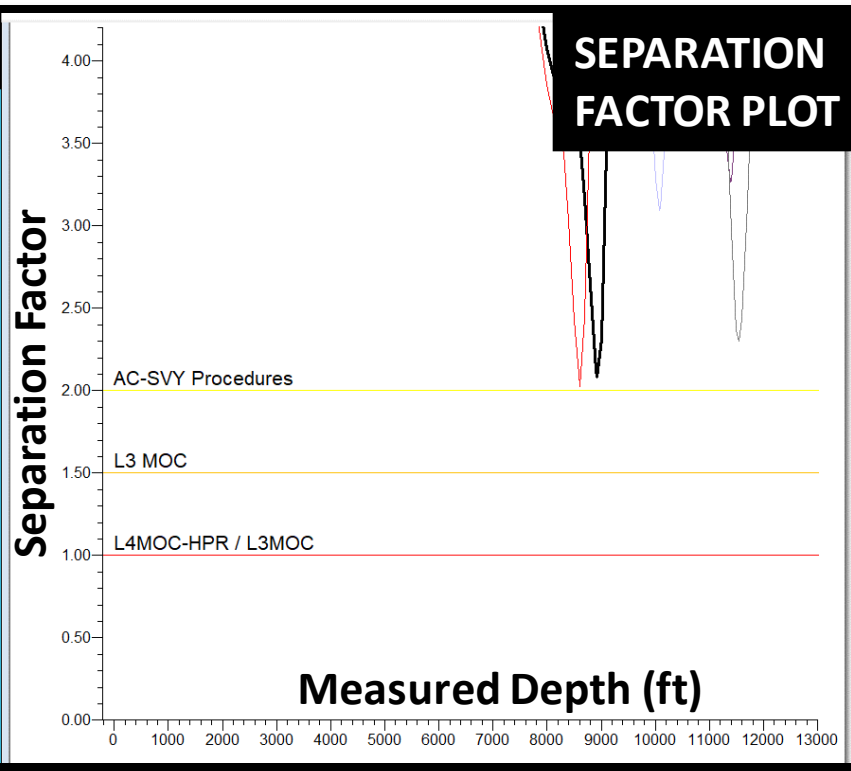
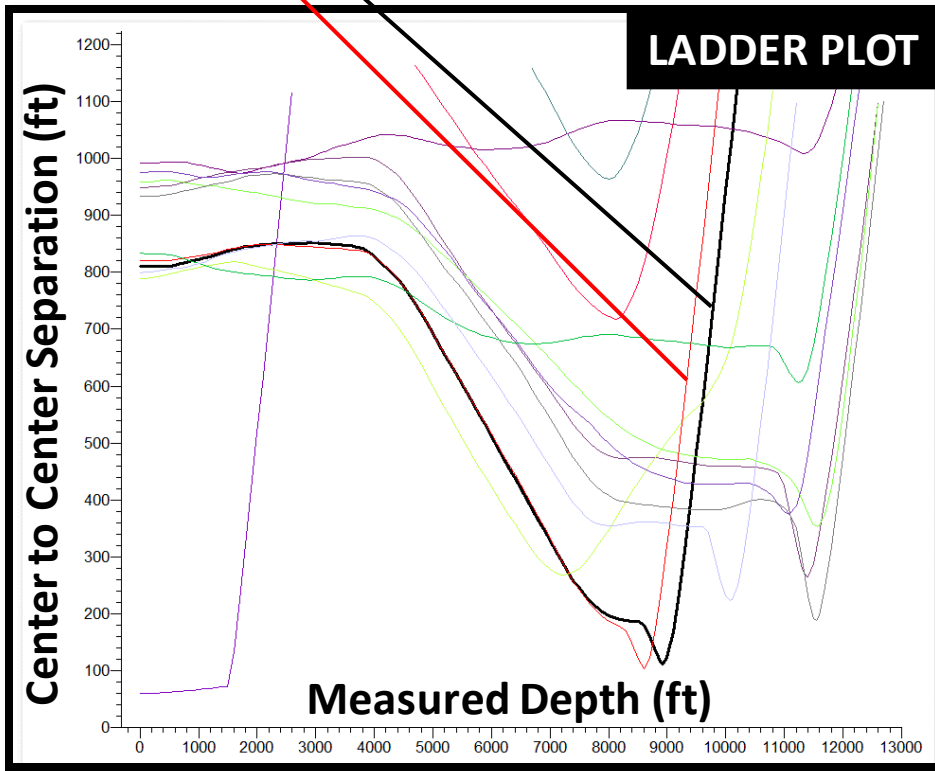
# Safe Separation Plots – Ladder & Separation Factor



# Safe Separation Plots – Ladder & Separation Factor

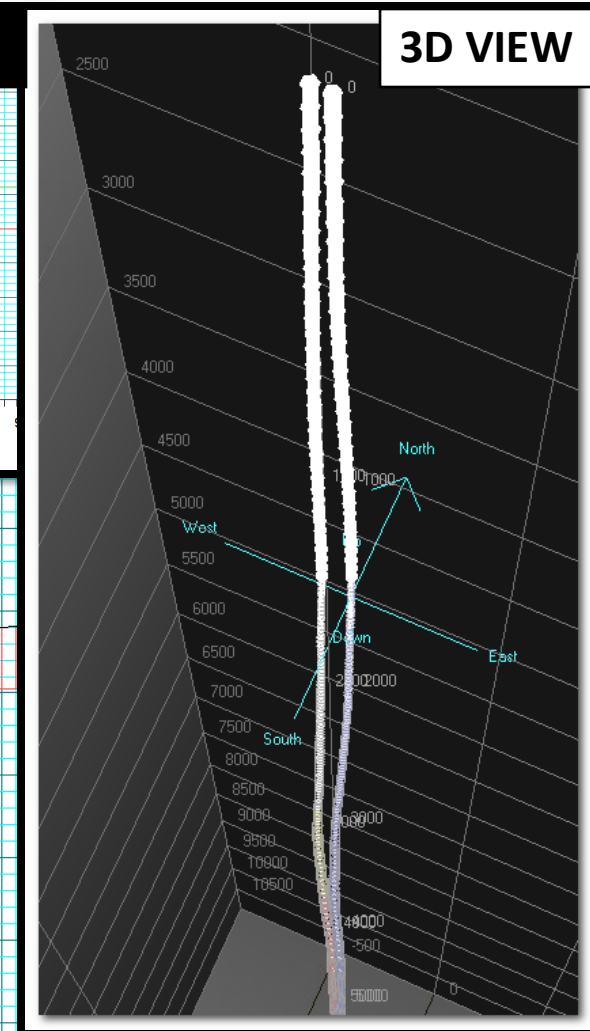
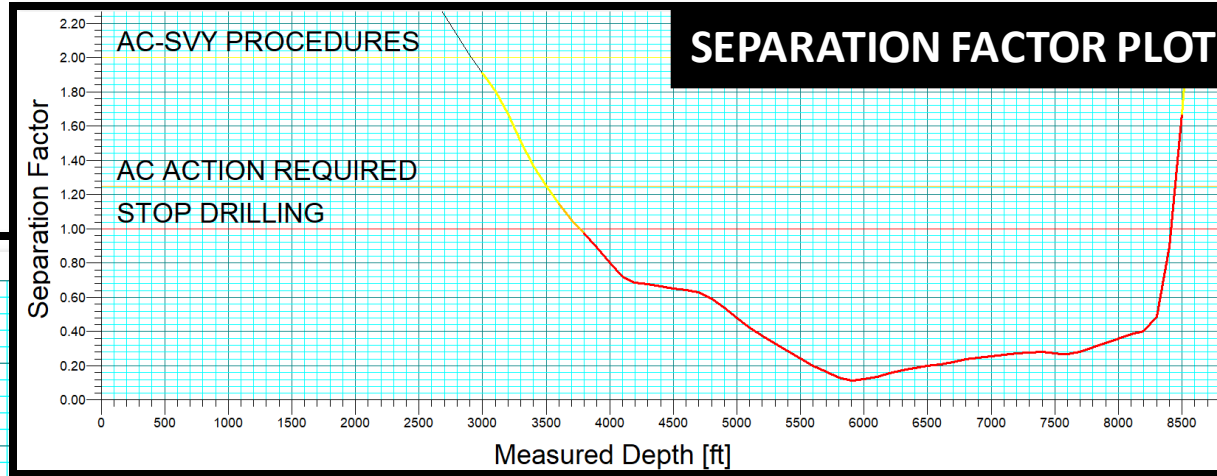


Offset B & C Indicates similar distance from planned well (Blue) which means these wellbore are very close from each other. They are neighboring slots on a four well pad drilled by another Operator.

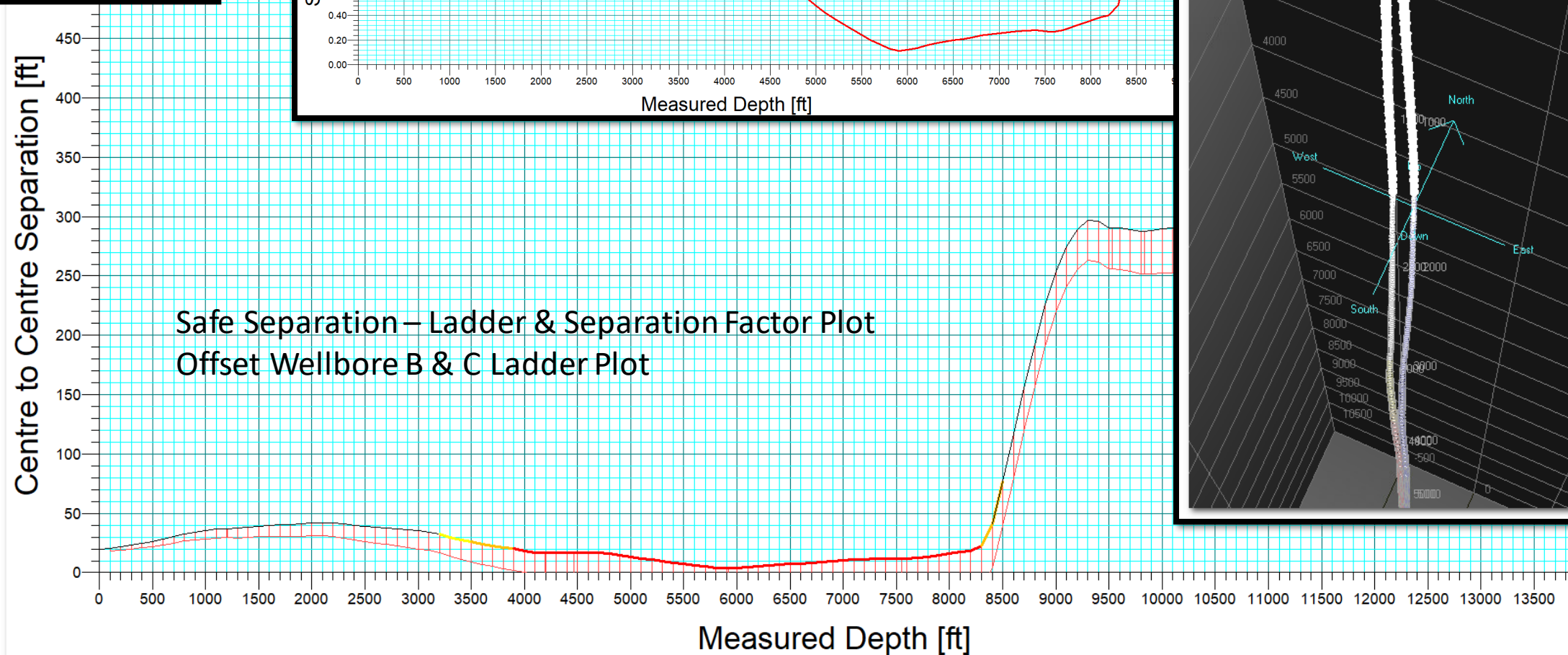




# Safe Separation Plots – Ladder & Separation Factor



## LADDER PLOT

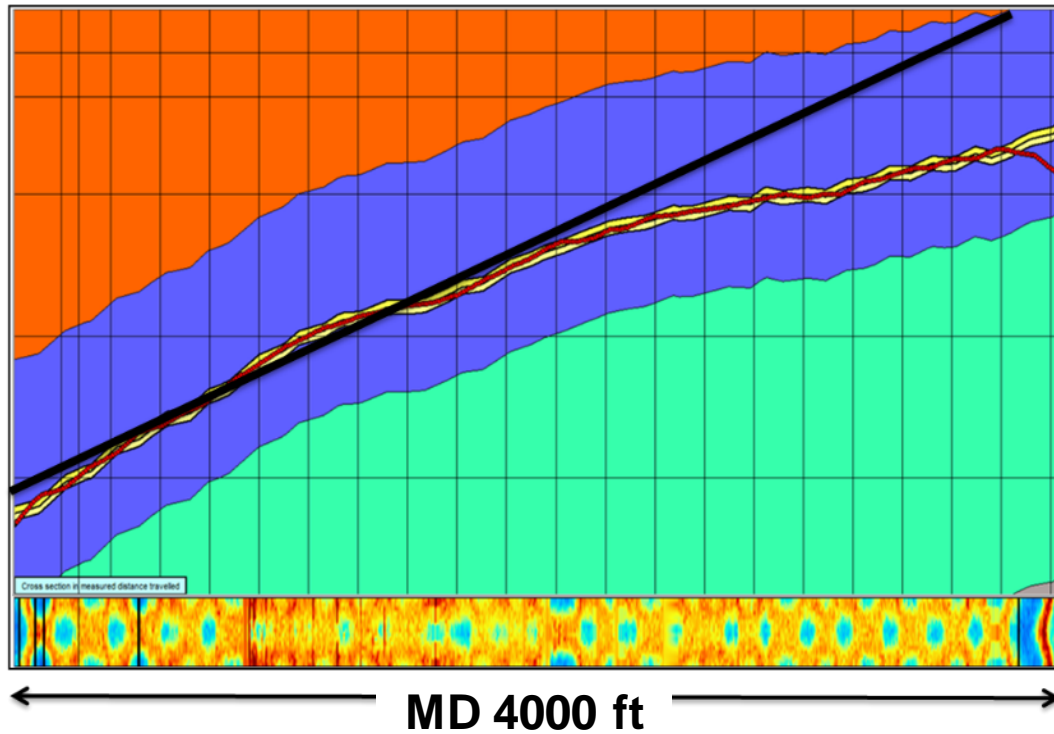


# Case Study

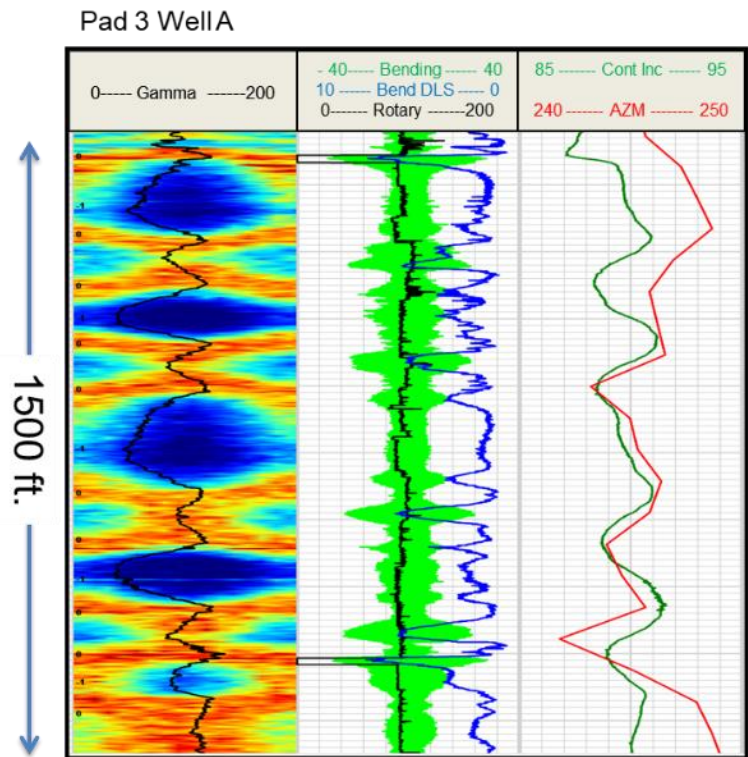
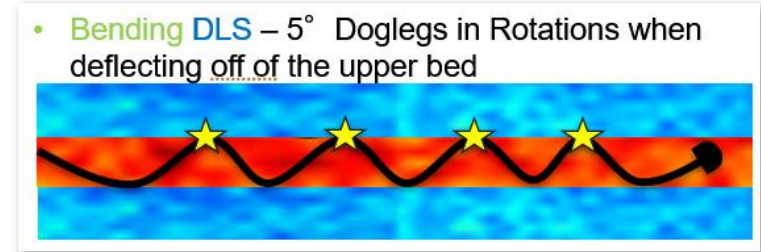
**Lateral Undulations**  
**Key Performance Indicators**  
**Steerable Motor Curve**  
**Lateral Tortuosity**



# Lateral Undulation Period - TVD Accuracy



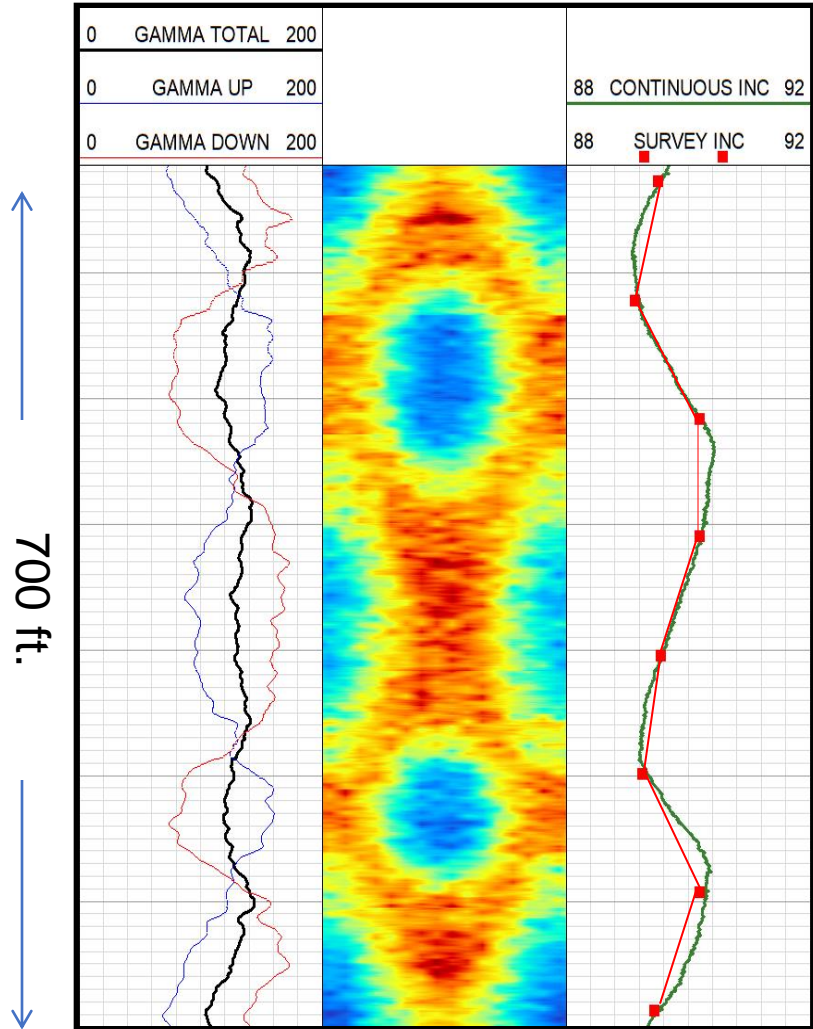
- What if the well plan diverges from the 'locked in' bed?
- If not identified then the DD may make a correction to go back to plan



Viens, Christopher , Clark, Tyler , Lightfoot, Jonathan , and Carlos Mercado. "Real-Time Downhole Data Resolves Lithology Related Drilling Behavior." Paper presented at the IADC/SPE Drilling Conference and Exhibition, Fort Worth, Texas, USA, March 2018. doi: <https://doi.org/10.2118/189697-MS>

# Lateral Undulation Period - TVD Accuracy

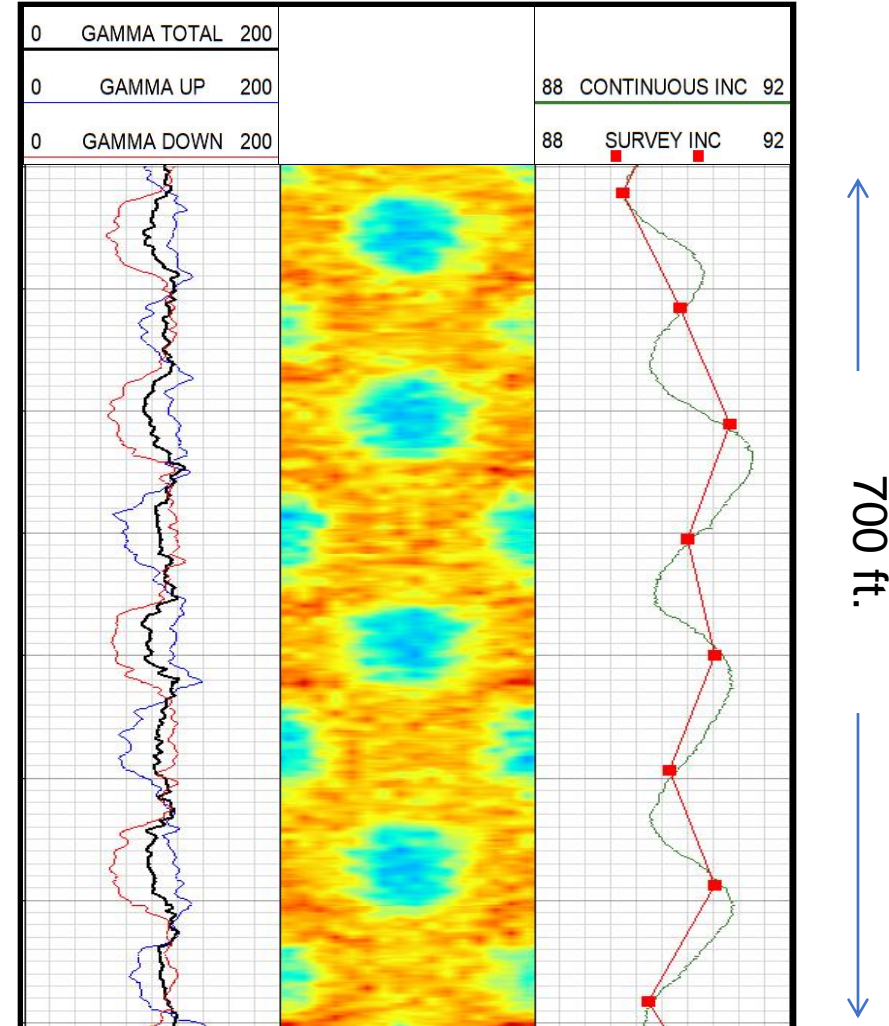
Pad 2 Well A



Left: 90' surveys adequate to due large period of oscillation

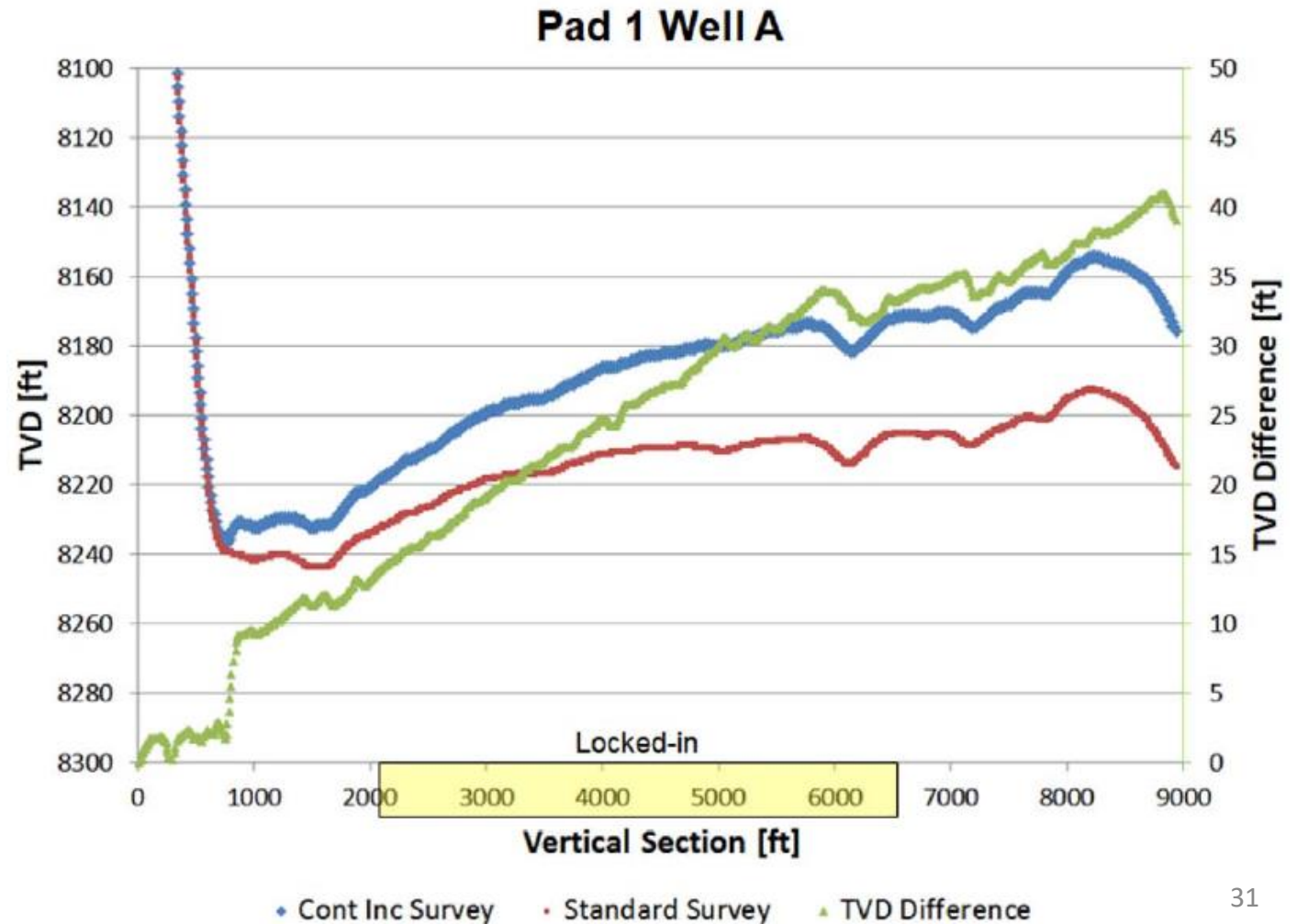
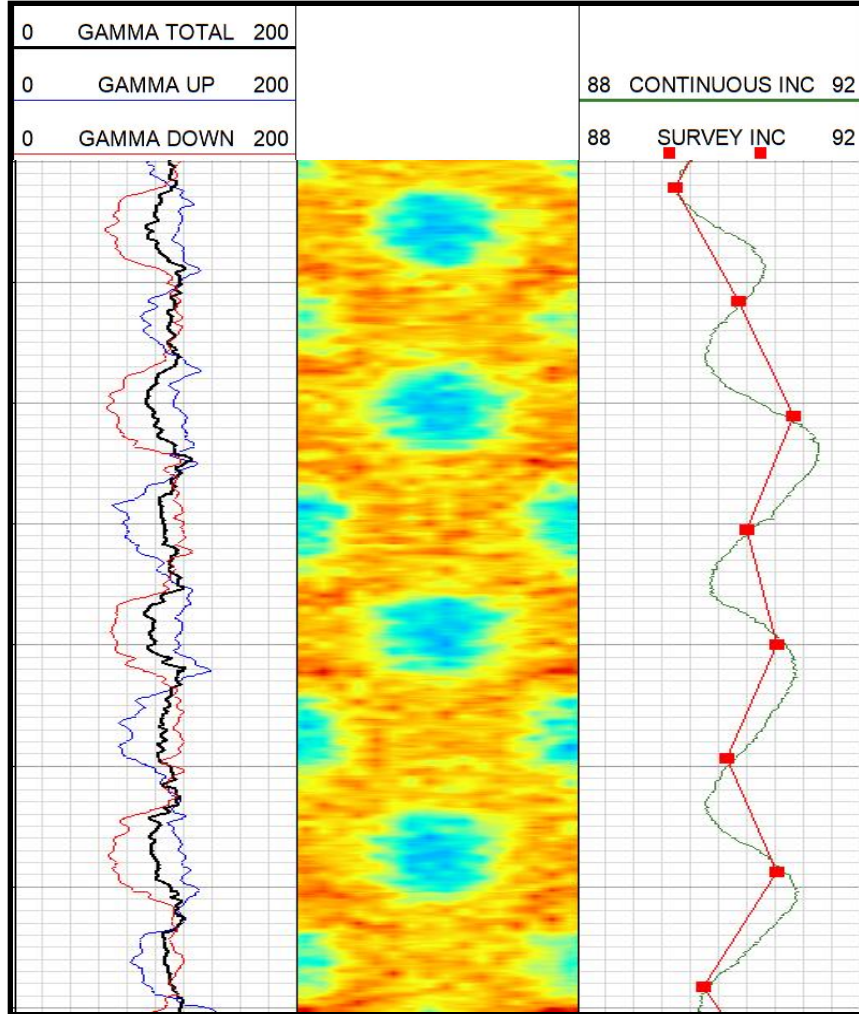
Right: 90' surveys inadequate to short oscillation period

Pad 1 Well A

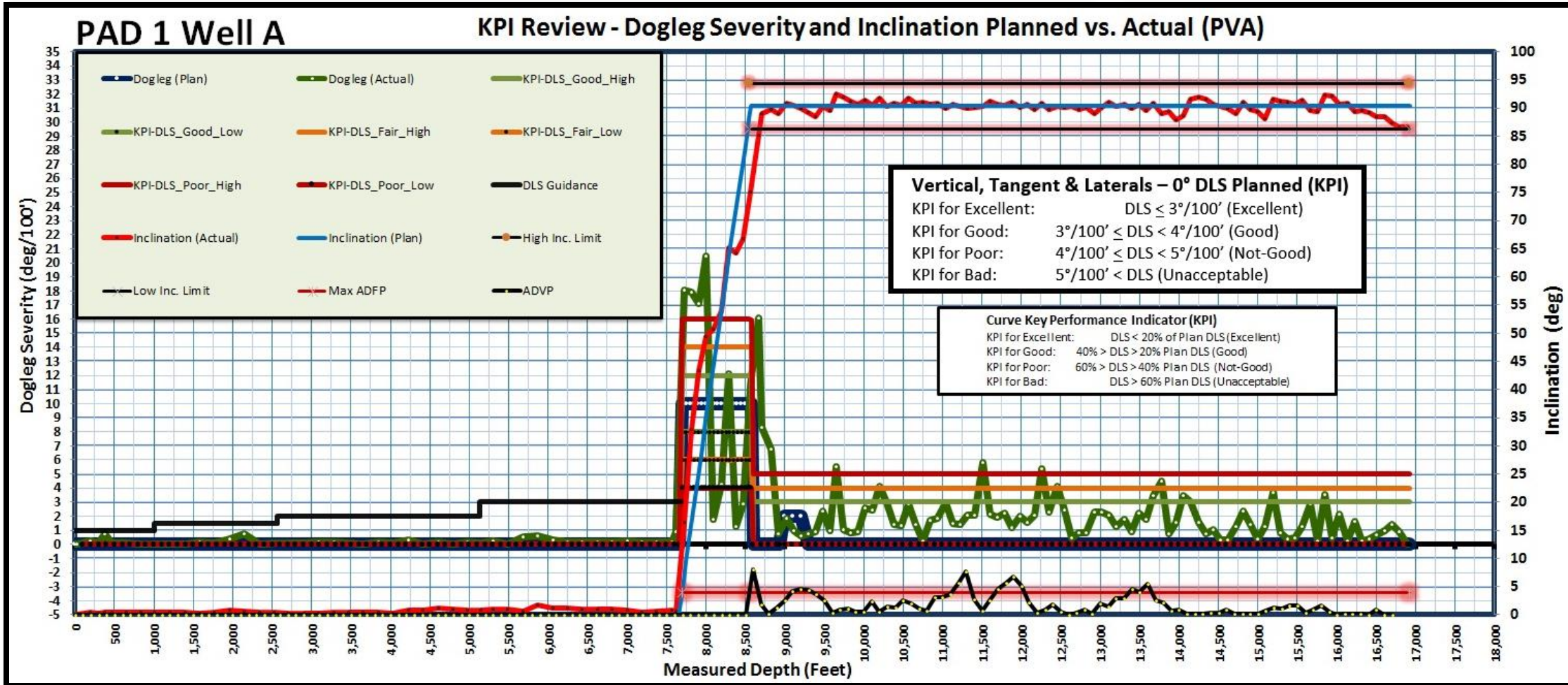


# Lateral Undulation Period - TVD Accuracy

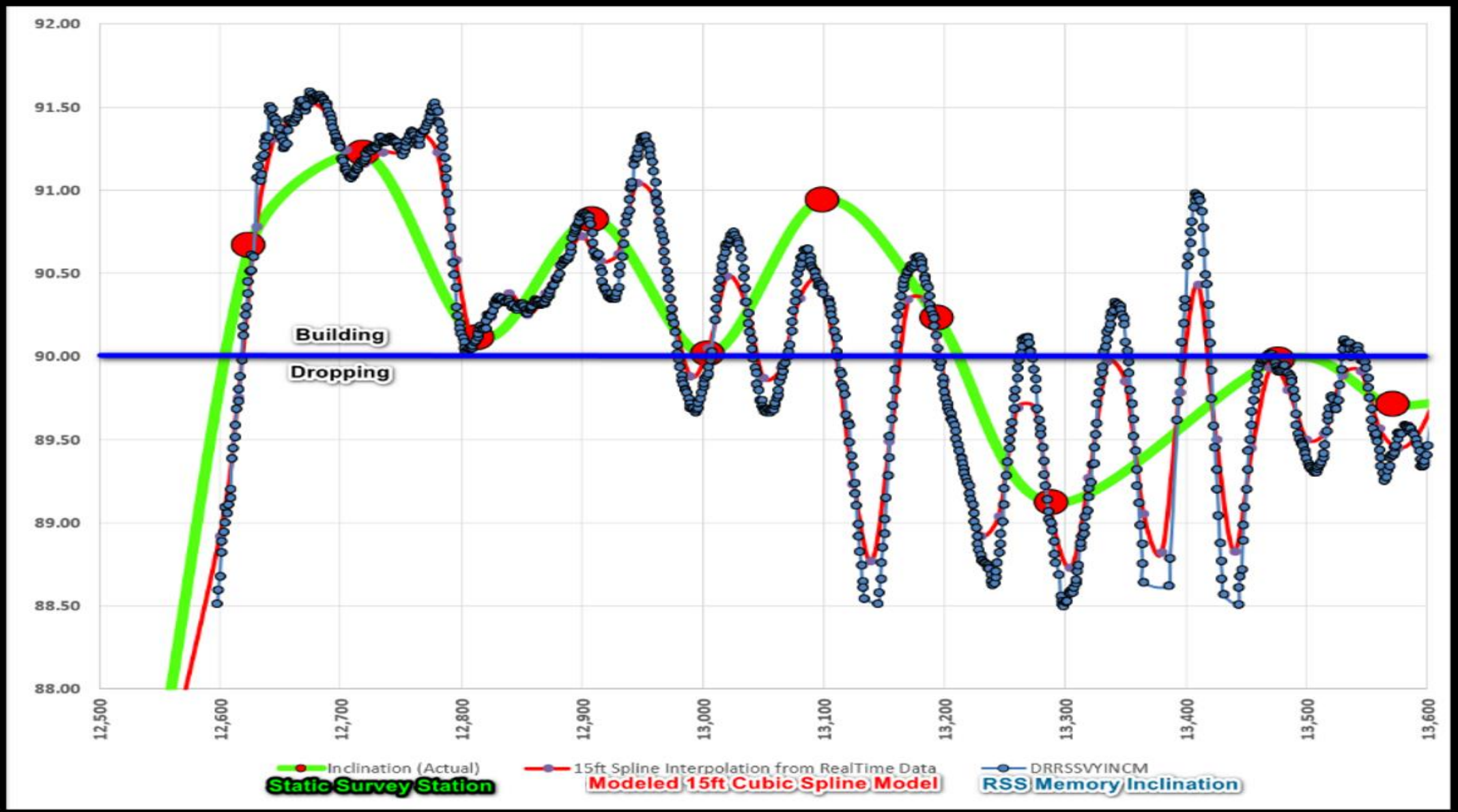
Pad 1 Well A



# Directional Drilling Key Performance Indicators



# Lateral Undulation Period – RSS Example



# Slide / Rotate Effect – Curve TVD Accuracy

Starting Survey = 10,000 ft MD

Inclination 30° & Azimuth 45°

- Case A: Slide 30 ft then Rotate 70 ft @ 10°/100'
- Case B: Rotate 70 ft then Slide 30 ft @ 10°/100'

Final Inclination 40° & Final Azimuth 45°

**Case A: Survey at 10,030' & at 10,100'**

- *DLS 16.7°/100 ft & TVD 9,082.6 ft*

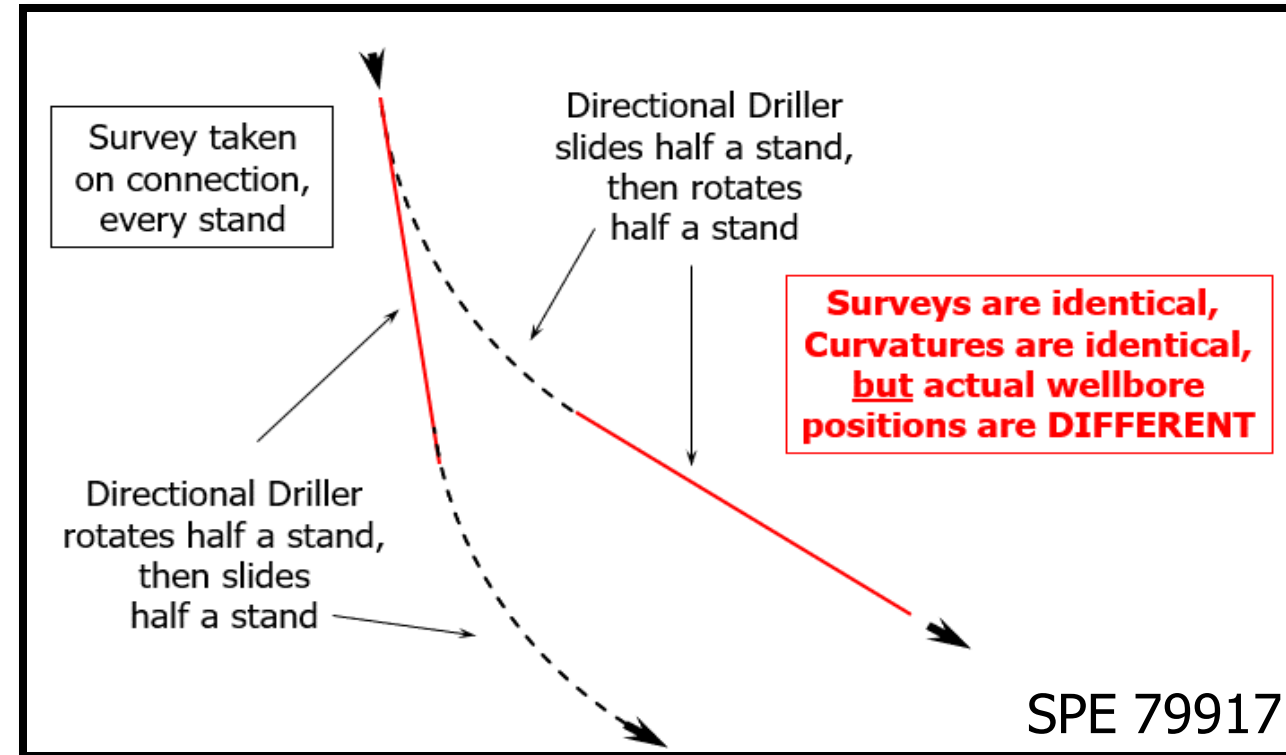
**Case B: Survey at 10,070' & at 10,100'**

- *DLS 16.67°/100 ft & TVD 9,085.9 ft*

**Case C: Survey only at 10,100'**

- *DLS 5°/100 ft & TVD 9,084 ft*

**Case A vs. Case B have a TVD difference  
3.29 ft over only 100 ft of MD (1-Stand)**





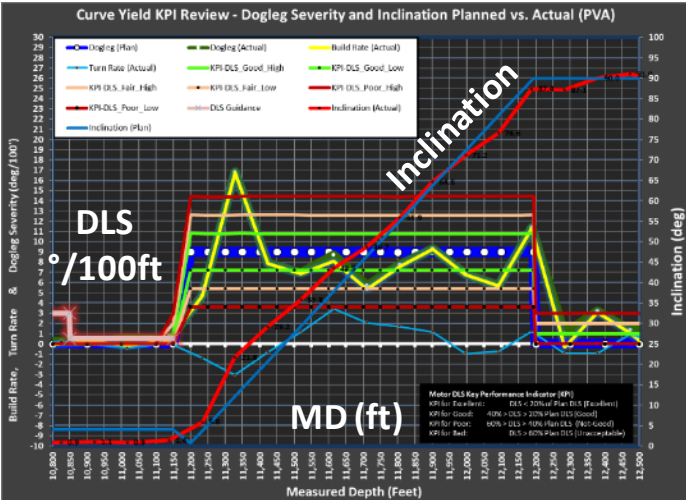
# Directional Drilling Key Performance Indicators



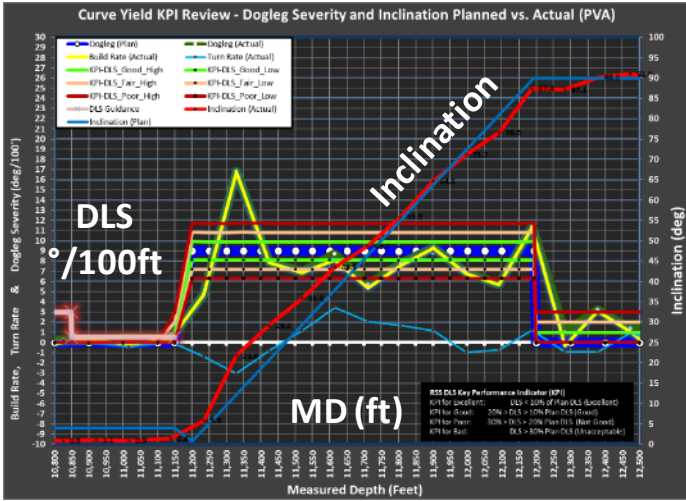
## Directional Drilling Dogleg Severity Control Key Performance Indicators

Directional Tools & Hole Section Type	Excellent	Good	Not-Good	Unacceptable RCRA Required
Vertical Intervals	$DLS \leq 2$	$2 < DLS \leq 3$	$3 < DLS \leq 4$	$4 < DLS$
Tangent Intervals	$DLS \leq 2$	$2 < DLS \leq 3$	$3 < DLS \leq 4$	$4 < DLS$
Lateral Intervals	$DLS \leq 2$	$2 < DLS \leq 3$	$3 < DLS \leq 4$	$4 < DLS$
Directional Motor Steering Interval	$DLS < +/- 20\%$ of Planned DLS	Between 20-40% of Planned DLS	Between 40-60% of Planned DLS	$DLS > +/- 60\%$ of Planned DLS
Directional RSS Steering Interval	$DLS < +/- 10\%$ of Planned DLS	Between 10-20% of Planned DLS	Between 20-30% of Planned DLS	$DLS < +/- 30\%$ of Planned DLS

### Offset Operator Motor Curve



Motor Curve KPI Chart  
20-40-60%



RSS Curve KPI Chart  
10-20-30%

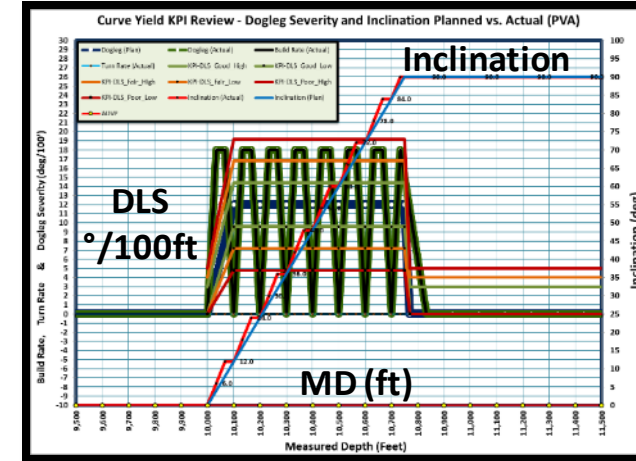
# Slide / Rotate Effect – Curve TVD Accuracy

Case A: Slide 33 ft, Rotate 33 ft and Slide 33 ft from 0° to 90° Inc.

MD	Inclination (Actual)	Azimuth (Actual)	Course Length	TVD	Vertical Section	+N / - S	+E / -W	Closure Distance	@ AZM	Dogleg (Actual)	Build Rate (Actual)	Turn Rate (Actual)
0.00	0.00	45.00	*****	0.00	0.00	0.00	0.00	0.00	45.00	0.00	*****	*****
10,000.00	0.00	45.00	10000.00	10000.00	0.00	0.00	0.00	0.00	45.00	0.00	0.00	0.00
10,033.33	6.00	45.00	33.33	10033.27	1.26	1.23	1.23	1.75	45.00	18.00	18.00	0.00
10,066.67	12.00	45.00	33.33	10066.18	5.03	4.92	4.92	6.96	45.00	18.00	18.00	0.00
10,100.00	18.00	45.00	33.33	10098.78	10.05	9.82	9.82	13.89	45.00	0.00	0.00	0.00
10,133.33	24.00	45.00	33.33	10130.97	16.29	15.92	15.92	22.51	45.00	18.00	18.00	0.00
10,166.67	30.00	45.00	33.33	10162.07	24.92	24.36	24.36	34.45	45.00	18.00	18.00	0.00
10,200.00	36.00	45.00	33.33	10192.52	34.73	33.95	33.95	48.01	45.00	0.00	0.00	0.00
10,233.33	42.00	45.00	33.33	10222.21	45.67	44.64	44.64	61.13	45.00	18.00	18.00	0.00
10,266.67	48.00	45.00	33.33	10250.15	58.80	57.47	57.47	74.82	45.00	18.00	18.00	0.00
10,300.00	54.00	45.00	33.33	10277.12	74.96	72.97	72.97	89.07	45.00	0.00	0.00	0.00
10,333.33	60.00	45.00	33.33	10301.01	93.15	89.91	89.91	103.88	45.00	18.00	18.00	0.00
10,366.67	66.00	45.00	33.33	10321.87	113.38	108.81	108.81	119.24	45.00	18.00	18.00	0.00
10,400.00	72.00	45.00	33.33	10348.87	135.56	129.33	129.33	144.24	45.00	0.00	0.00	0.00
10,433.33	78.00	45.00	33.33	10369.84	159.64	153.64	153.64	169.06	45.00	18.00	18.00	0.00
10,466.67	84.00	45.00	33.33	10387.99	185.66	178.40	178.40	224.01	45.00	18.00	18.00	0.00
10,500.00	90.00	45.00	33.33	10404.66	213.54	205.81	205.81	282.87	45.00	0.00	0.00	0.00
10,533.33	90.00	45.00	33.33	10419.78	244.27	235.80	235.80	345.37	45.00	0.00	0.00	0.00
10,566.67	90.00	45.00	33.33	10431.72	276.92	265.79	265.79	413.67	45.00	18.00	18.00	0.00
10,599.99	90.00	45.00	33.33	10442.02	310.86	294.21	294.21	486.37	45.00	0.00	0.00	0.00
10,633.33	90.00	45.00	33.33	10450.64	346.14	321.97	321.97	563.55	45.00	18.00	18.00	0.00
10,666.67	90.00	45.00	33.33	10455.86	382.94	346.24	346.24	645.46	45.00	18.00	18.00	0.00
10,699.99	90.00	45.00	33.33	10459.34	420.33	369.68	369.68	731.61	45.00	0.00	0.00	0.00
10,733.33	90.00	45.00	33.33	10461.08	458.30	391.20	391.20	821.88	45.00	18.00	18.00	0.00

Case A Directional Survey

SIMULATED EXAMPLE

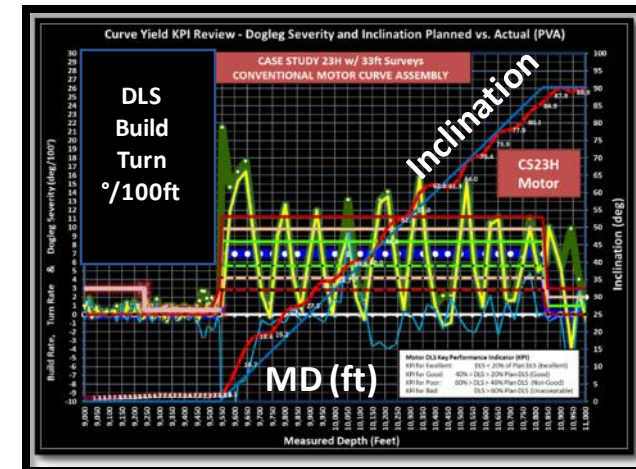


Case B: Survey Every 100 ft from 0° to 90° Inc. (16 ft TVD Delta)

MD (Plan)	Inclination (Plan)	Azimuth (Plan)	Course Length	TVD	Vertical Section	+N / - S	+E / -W	Closure	@ AZM	Dogleg (Plan)	Build Rate	Turn Rate
0.00	0.00	0.00	*****	0.00	0.00	0.00	0.00	0.00	0.00	0.00	*****	*****
10,000.00	0.00	45.00	10000.00	10,000.00	0.00	0.00	0.00	0.00	45.00	0.00	0.00	0.45
10,100.00	10.00	45.00	100.00	10,099.17	7.55	7.38	7.38	1.43	45.00	12.00	12.00	0.00
10,200.00	20.00	45.00	100.00	10,197.43	14.95	14.56	14.56	2.88	45.00	12.00	12.00	0.00
10,300.00	30.00	45.00	100.00	10,293.64	22.48	21.85	21.85	4.39	45.00	12.00	12.00	0.00
10,400.00	40.00	45.00	100.00	10,388.83	30.14	29.27	29.27	5.94	45.00	12.00	12.00	0.00
10,500.00	50.00	45.00	100.00	10,483.00	37.93	36.71	36.71	7.51	45.00	12.00	12.00	0.00
10,600.00	60.00	45.00	100.00	10,576.14	45.84	44.27	44.27	9.09	45.00	12.00	12.00	0.00
10,700.00	70.00	45.00	100.00	10,668.14	53.87	51.74	51.74	10.68	45.00	12.00	12.00	0.00
10,800.00	80.00	45.00	100.00	10,759.00	62.02	59.53	59.53	12.28	45.00	12.00	12.00	0.00
10,900.00	90.00	45.00	100.00	10,848.74	70.28	67.40	67.40	13.89	45.00	12.00	12.00	0.00
10,950.00	90.00	45.00	50.00	10,847.46	345.42	337.62	337.62	477.46	45.00	12.00	12.00	0.00

Case B Directional Survey

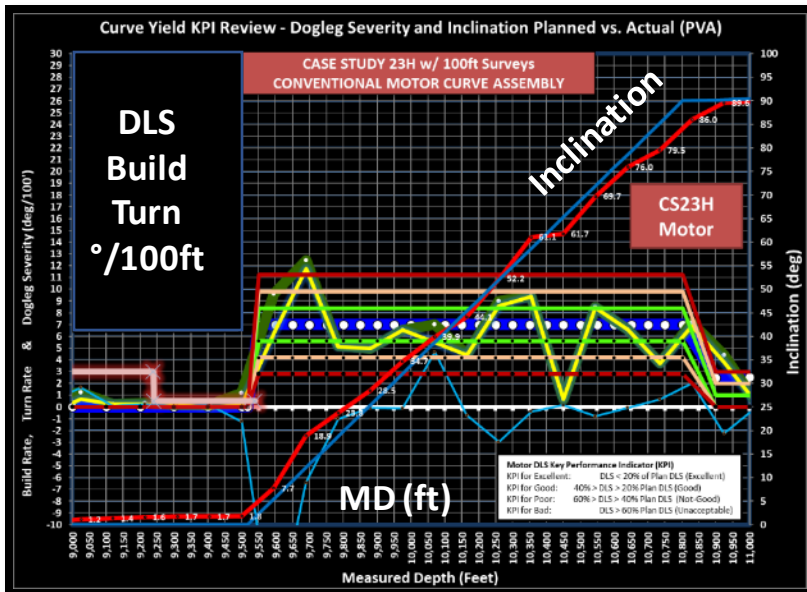
ACTUAL EXAMPLE



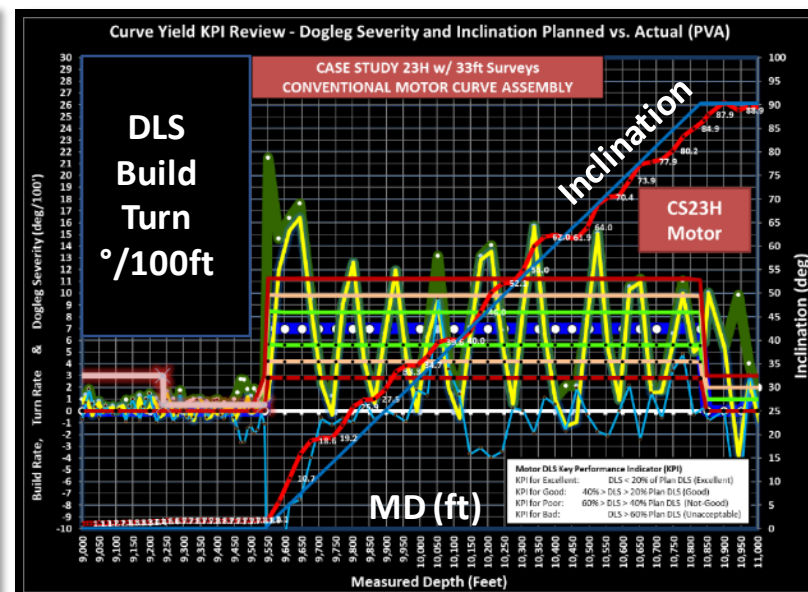
# Case Study - Steerable Motor Curve

- Survey Frequency is Important for Medium Radius Curves
- If slide % is less, consider surveying twice a stand or every joint
- When sliding 90 to 100%; survey is less prone to landing TVD error

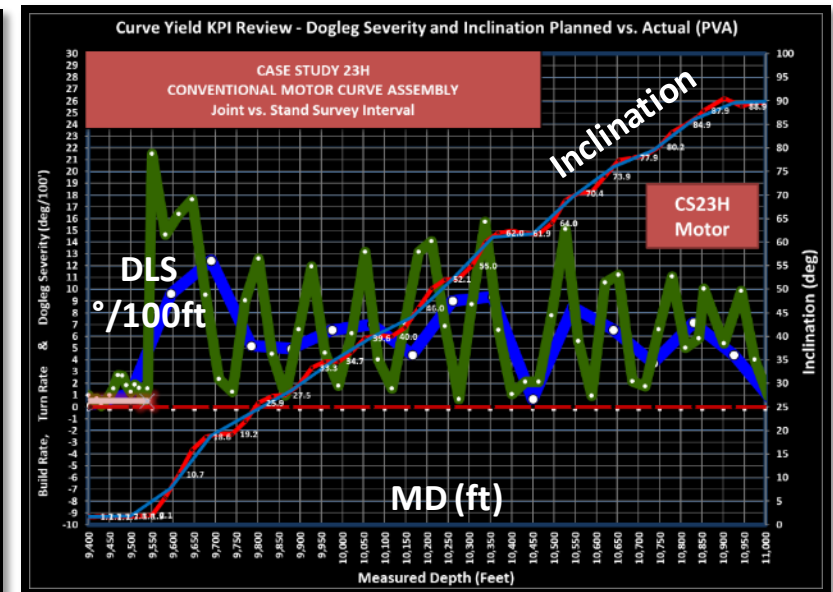
96 FT SURVEYS



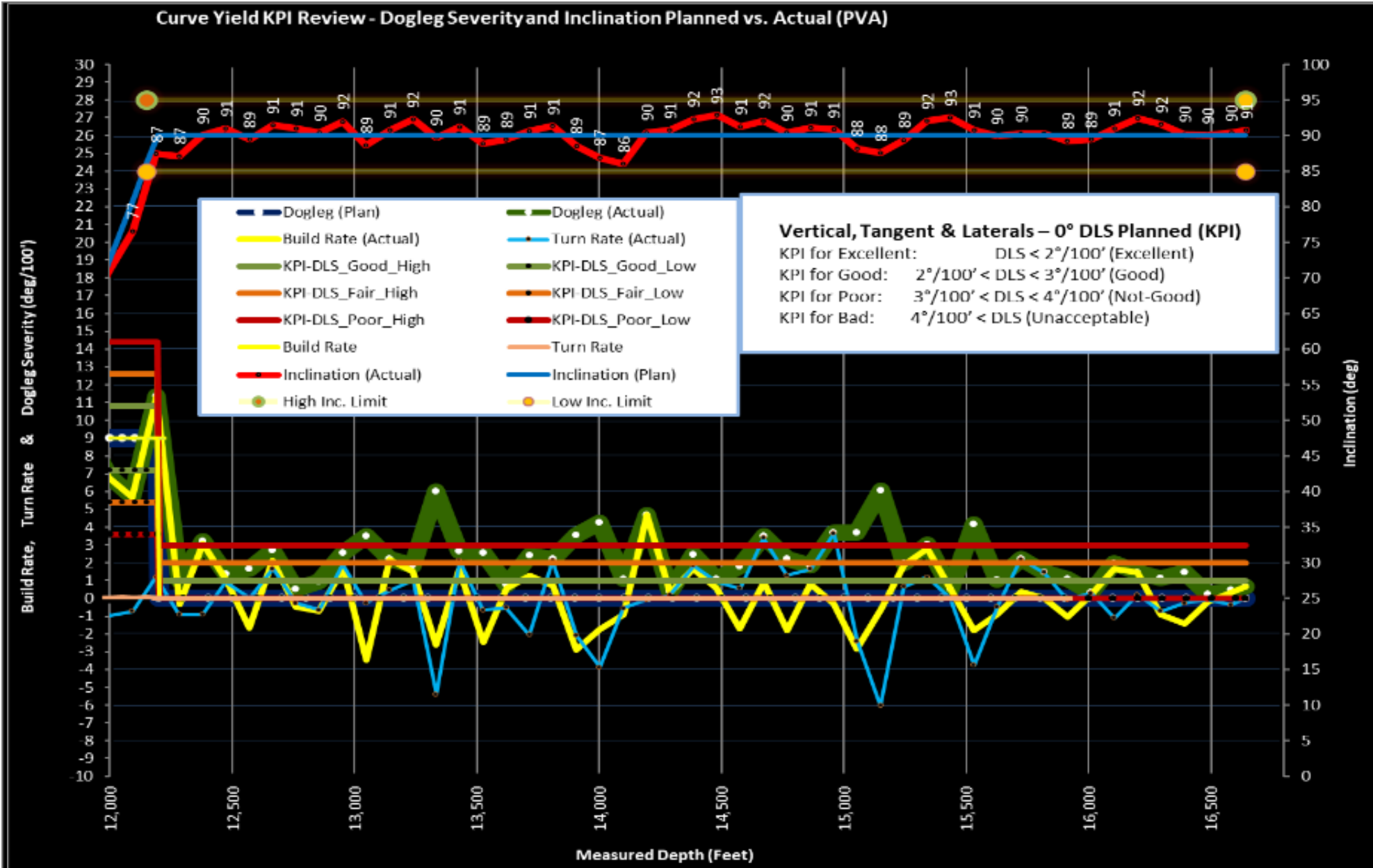
32 FT SURVEYS



DLS COMPARISON



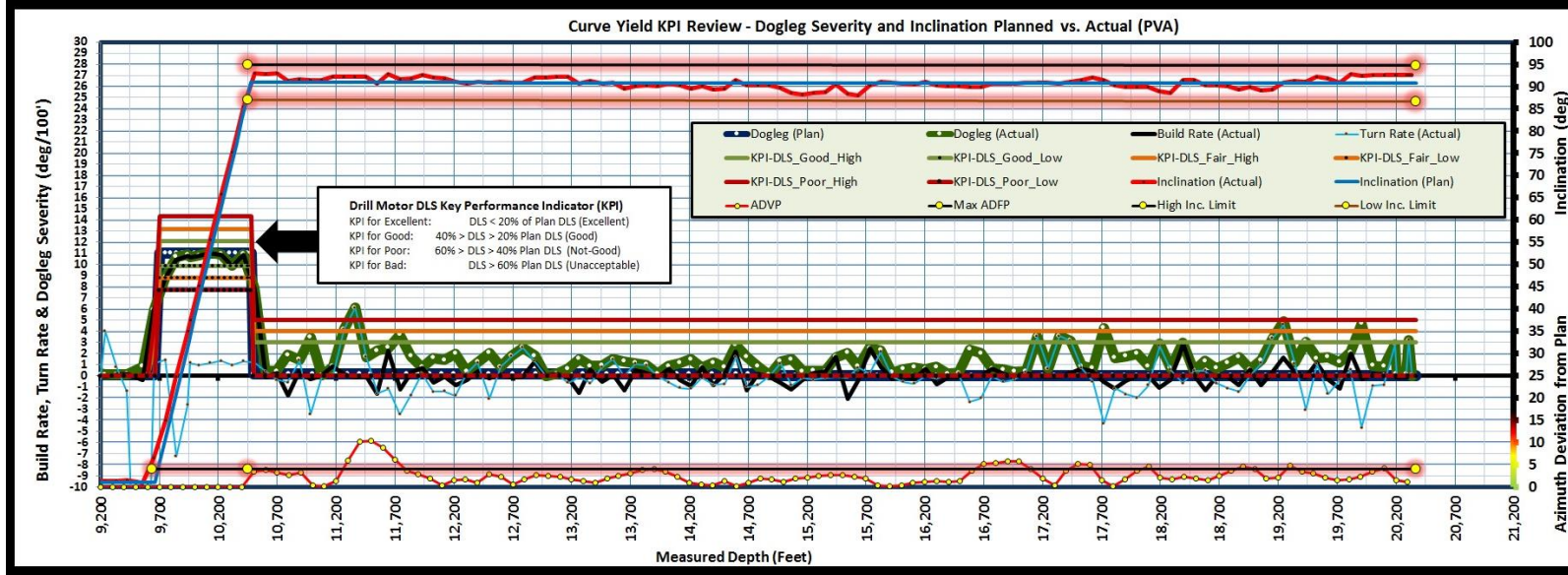
# Lateral Tortuosity KPI – Case Study



Lateral DLS  
Build & Turn  
Rate KPI Chart  
With Inclination  
+/- Allowable  
Deviation from  
Plan

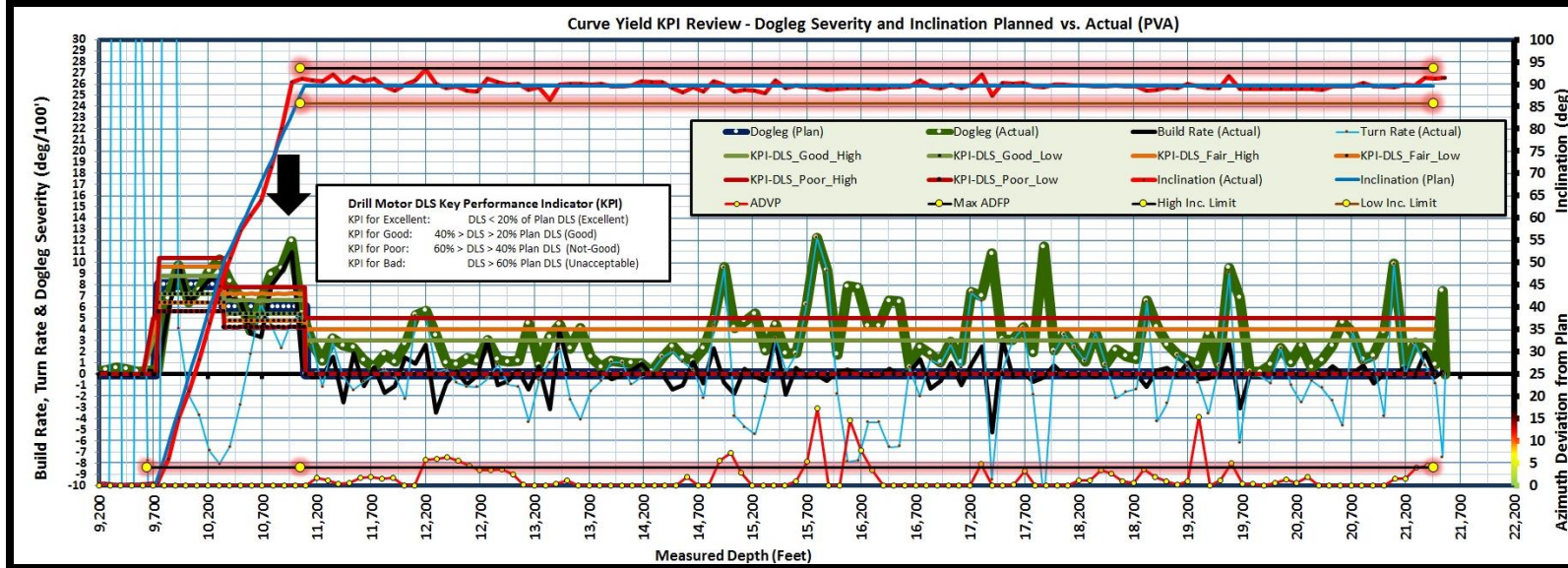
Surface  
to TD DLS  
KPI Chart with  
Artificial Lift DLS  
Guidance for  
Surface &  
Intermediate

# Case Study – RSS Low Tortuosity



Curve Lateral  
Tortuosity KPI  
RSS Examples

# Case Study – RSS High Tortuosity



# Key Takeaways

- As demonstrated in these case studies, Safe Separation collision avoidance methods are designed to safely separate wellbores while also improving wellbore position accuracy.
- The survey interval should be considered during both the drilling planning and execution phases.
- Key performance indicators aid in achieving the objectives and expectations of directional wells.
- Wellbore Surveying and Positioning Practices
  - Provides a primary source of technical information for all subsurface borehole construction applications.
  - Contributes to the modernization of the wellbore construction industry by promoting safe separation procedures.
  - All participants in wellbore construction should support the collaborative effort of a committed group of industry volunteers. The desired outcome is industry-wide adoption.

See the WPTS for more information: <https://connect.spe.org/wellborepositioning>

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